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Heat treatment of silanized feldspathic ceramic: Effect on the bond strength to resin after thermocycling



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ABSTRACT

Purpose: This study aimed to evaluate the effect of heat treatment (at 77 °C) of a silanized feldspathic ceramic on microtensile bond strength (μ TBS) with a resin cement before and after being aged by thermocycling.

Material and methods: Twenty-four blocks ($12 \times 10 \times 4$ mm³) of a CAD/CAM feldspathic ceramic (Vita-blocks Mark II, Vita) were obtained and randomly divided into three groups, according to the surface treatment prior to the cementation: Group AS – hydrofluoric acid 10%+silane; Group S77 – silane+heating at 77 °C for 60 s; and Group AS77 – hydrofluoric acid 10%+silane+heating at 77 °C for 60 s. Ceramic blocks were cemented to composite resin blocks with a resin cement. The sets were subsequently cross-sectioned into 1 mm² beams for μ TBS testing. The beams of each group were randomly divided into two subgroups: aging (thermocycling, 12,000 cycles between 5 °C and 55 °C) and non-aging (tested immediately). One-way ANOVA and Tukey's test ($\alpha=0.05$) and Weibull analysis (95% CI) were used to analyze the data.

Results: Group AS77 had the lowest pre-test failure number during the cutting among the groups. There was no significant difference ($p=0.255$) between the μ TBS mean values of the non-aged groups. After aging, the mean value of S77 was significantly lower than those of AS77 and AS ($p=0.005$). There was no difference in the Weibull modulus (m) and characteristic strength (σ_0) of the aged and non-aged groups for all comparisons. Before aging, heat treatment of silanized feldspathic ceramic (non acid-etched surface) demonstrated bond strength similar to that achieved with hydrofluoric-acid-etching treatment however, it had lower bond strength after aging.

Conclusion: The combination of hydrofluoric-acid-etching treatment with heat treatment silanized feldspathic ceramic did not improve the bond strength of the interface.

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1. Introduction

Feldspathic ceramic has been used in dental restorations mainly due to the excellent long-term esthetics provided by its color stability. The established surface treatment for this class of ceramic to bond with resin cements is the 'hydrofluoric acid etching+silane coupling agent application' [1–3]. Surface etching with hydrofluoric acid promotes roughness on the ceramic [1],

favoring micromechanical interlocking, and also improves the wettability of the silane on the ceramic surface, by energy surface modification [4]. Nevertheless, the use of hydrofluoric acid has been questioned in some studies, mainly due to its chemical toxicity and hazardous effects, but also due to the formation of insoluble salts that can affect bond strength [3,5–11]. Therefore, alternative treatments for bonding to these ceramics have been proposed, as silane heating in air stream [5,6,12,13] or oven [14–17], and bath in hot water [17]. These temperature-based treatments have the ability to eliminate solvents of the material and enhance the crosslink reaction, favoring the bonding [17].

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The silane coupling agent consists of a bifunctional molecule with an organic side (reacts with resins and promotes the formation of oligomers) and an inorganic side (reacts with metal oxides and silica of the ceramic glass phase). This characteristic is responsible for cement/ceramic chemical bonding [1,3,4,6,18]. The greater the interaction of the silane molecules on the ceramic surface, the better the bond strength of the system and the resistance to degradation of the silane film [18,19]. After final condensation, the silane film is basically composed of three structurally and physico-chemically different layers: (a) an outer layer, in which silane molecules are weakly attached, with few siloxane bonds that are easily hydrolyzed and removed; (b) a middle layer, in which molecules have strong siloxane bonds that are more resistant to hydrolysis and can be removed only with a hot water bath; and (c) an inner layer, in which the silane is considered chemically reactive [20].

Studies testing the bond strength of the ceramic/resin interface have shown positive results of heat treatment of the silane layer before cementation [5,6,8,12,15,17,21]. Specifically, silane heat treatment at 77 °C (solvent evaporation temperature) increased the bond strength between the ceramic and resin cement compared with that achieved by conventional treatment, even after mechanical aging, showing the stability of the technique after short-term mechanical cycling [17]. However, the literature lacks studies concerning the real effect of temperature (hot air without the association of an air spray), mainly after aging by thermocycling, on the bond strengths between feldspathic ceramic and resin cement. Moreover, the association of heat treatment with the conventional protocol after aging, designed to improve bond strength, should be tested. Therefore, the aim of this study is to evaluate the effect of a 77 °C heat treatment of a silanized feldspathic ceramic on the microtensile bond strength (μ TBS) with a resin cement before and after being aged by thermocycling. The null hypotheses are: (1) the heat treatment does not affect the bond strength; (2) the combination of the hydrofluoric-acid-etching treatment with heat treatment does not improve the bond strength; and (3) the thermocycling does not affect the reliability of the interfaces.

2. Materials and methods

2.1. Materials of study

The materials used in this study are described in Table 1.

2.2. Specimen preparation

Six blocks of a feldspathic ceramic for CAD/CAM (Vitablocks Mark II) with dimensions of $12 \times 10 \times 17 \text{ mm}^3$ were sectioned in a cutting machine (Isomet 1000, Buehler Ltd., Lake Bluff, IL, USA), resulting in 24 ceramic blocks ($12 \times 10 \times 4 \text{ mm}^3$). All blocks were ground-finished for surface standardization with 600-grit wet silicon carbide

papers (3M ESPE, St. Paul, MN, USA). The blocks were molded using a silicone impression material (Elite HD, Zhermack, Badia-Polesine, Rovigo, Italy), and the mold was used to the construction of the composite resin blocks (Z100, A1 shade) which were cemented onto the ceramic surfaces. The composite resin was incrementally applied to the mold (2 mm thickness for each increment), and each increment was light-cured for 40 s (XL 3000, 3M/ESPE; light intensity = 500 mW/cm^2) at a distance of 10 mm, until the total fulfillment of the mold. Light intensity was verified by radiometry so that it was no lower than 500 mW/cm^2 . The composite resin blocks were made on the day of cementation. The final dimension of the composite resin blocks was similar to the ceramic blocks.

2.3. Surface treatment

The ceramic blocks were ultrasonically cleaned in distilled water for 5 min, and randomly divided into three groups, according to the surface treatment:

- Group AS – The ceramic surface was etched with 10% HF for 60 s, washed, and air-dried for 30 s. The silane coupling agent was applied by means of a microbrush (3M ESPE) for 60 s and gently dried with air spray for 15 s.
- Group S77 – The silane coupling agent was applied to the surface by means of a microbrush for 60 s and gently dried with air spray for 15 s. The silanized block was placed in a 77 °C preheated oven for 60 s.
- Group AS77 – The ceramic surface was etched with 10% HF for 60 s, washed, and air-dried for 30 s. The silane coupling agent was applied by means of a microbrush for 60 s and gently dried with air spray for 15 s. The silanized block was placed in a 77 °C preheated oven for 60 s.

2.4. Specimens cementation

After the treatments, the blocks of resin composite were cemented onto the ceramic blocks by means of a resin cement (Variolink II), with a constant pressure of 750 g for 60 s. The excess cement was removed, and the set was light-cured for 40 s on each side. All sets were stored in distilled water at 37 °C for 24 h before the sticks obtaining.

2.5. Beams preparation

The ceramic/resin sets were embedded in chemically cured acrylic resin, positioned in a cutting machine (Isomet, Buehler), and sectioned at low speed with water cooling. Each set was longitudinally cut into a series of 1.0-mm-thick slices and then rotated 90° for a second sectioning. Approximately 68 beams with (cross-section, area of 1.0 mm^2) were obtained from each set. The edge sections (measuring approximately 1 mm) were discarded due to the possibility of excess or no cement at the interface,

Table 1

Brand name, material type, manufacturer and composition of the materials used in the study.

Brand name	Material type	Manufacture	Composition
Vitablocks Mark II	Feldspathic ceramic	VITA Zanhfabrik; Bad Säckingen, Germany	Feldspathic cristaline particles (SiO_2 , Al_2O_3 , Na_2O , K_2O) in glassy matrix
Monobond S	Silane coupling agent	Ivoclar Vivadent; Schaan, Leichtenstein	1% 3-methacryloxypropyl trimethoxysilane (3-MPS) ethanol/water-based solvent
Porcelain Conditioner	Acid etchant	Dentsply; Petropolis, Brasil	Hydrofluoric acid (HF) 10%
Variolink II	Resin Cement	Ivoclar Vivadent, Schaan, Leichtenstein	Monomer matrix: Bis-GMA, urethane, dimethacrylate and triethylene glycol dimethacrylate. Inorganic fillers: barium glass, ytterbium trifluoride, Ba-Al-fluorosilicate glass and spheroid mixed oxide
Z100	Composite resin	3M ESPE; St Paul, MN, USA	Bis-GMA, TEGDMA, zirconia/silica (0,6 μm)

which could alter the results. The specimens from each set of ceramic/resin were randomly divided into two subgroups: aging and non-aging. Aging was performed in a thermocycling machine (MSCT-3 Plus, Erios, São Paulo, Brazil): 12,000 cycles were completed between 5 ± 1 °C and 55 ± 1 °C, with 30 s for each bath. The specimens that were not subjected to the aging process were tested immediately after being sectioned.

2.6. Microtensile bond strength test

The beams' bonding area was measured with a digital caliper (Starret Industria e Comercio Ltda, Itu, Brazil). Each beam was fixed to a testing device by means of cyanoacrylate gel (Super Bonder Gel, Loctite Ltda, São Paulo, Brazil) as parallel as possible to the long axis of the device, which was fixed in a universal testing machine (DL-1000, EMIC, São José dos Pinhais, Brazil). The beams were loaded for tensile testing at a crosshead speed of 1 mm/min with a 50 kgf load cell until failure. Microtensile bond strength (μ TBS) was calculated according to the equation $R=F/A$, where R is the strength (MPa), F is the load (N) required to fracture the specimen, and A is the bonding area (mm^2).

2.7. Failure analysis

The fractured sticks were analyzed by stereomicroscopy (Discovery V-20, Carl Zeiss, Göttingen, Germany), and representative beams were examined by scanning electron microscopy (Inspect S50, FEI Company, Orlando, EUA). The fracture types were classified

Table 2

Number of blocks and sticks of the experimental groups, number and percentage of pre-test failures (PTF) during cutting and during aging, and total number of beams tested.

Group	Blocks	Beams	PTF during cutting	Aging	PTF during aging	Beams tested
AS77	8	524 (100%)	171 (32.6%)	No	–	178 (34.0%)
				Yes	0	175 (33.4%)
AS	8	558 (100%)	272 (48.7%)	No	–	170 (30.5%)
				Yes	0	116 (20.8%)
S77	8	568 (100%)	302 (53.2%)	No	–	146 (25.7%)
				Yes	0	120 (21.1%)

Table 3

Comparisons of the nonaged groups: number and percentage of adhesive, cohesive and mixed failures; mean and standard deviation (SD) of the values of adhesive failure and p -value for the comparison*; Weibull modulus (m) and characteristic strength (σ_0) values with the confidence intervals (CI).

Group	Type of failure			Bond strength (* $p=0.255$)	Weibull analysis	
	Adhesive	Cohesive	Mixed		m (CIs)	σ_0 (CIs)
AS77	144 (80.9%)	8 (4.5%)	26 (14.6%)	19.1 (7.6)	2.9 (2.5–3.2)	21.9 (20.6–23.1)
AS	133 (78.2%)	36 (21.7%)	1 (0.1%)	18.5 (11.0)	1.9 (1.6–2.3)	21.8 (19.5–24.2)
S77	100 (68.5%)	36 (24.6%)	10 (6.9%)	18.0 (7.8)	2.6 (2.2–3.0)	20.7 (18.9–22.2)

* The bond strength data of the groups were not statistically different (One-way Anova comparison, $\alpha=0.05$).

Table 4

Comparisons of the aged groups: number and percentage of adhesive, cohesive and mixed failures; mean and standard deviation (SD) of adhesive failure values, p -value and grouping information*; Weibull modulus (m) and characteristic strength (σ_0) values with the confidence intervals (CI).

Group	Type of failure			Bond strength (* $p=0.005$)	Weibull analysis	
	Adhesive	Cohesive	m (CIs)		m (CIs)	σ_0 (CIs)
AS77	146 (83.4%)	17 (9.7%)	12 (6.9%)	16.8 (7.4) a	2.5 (2.2–2.8)	19.1 (17.7–20.3)
AS	85 (73.3%)	26 (22.4%)	5 (4.3%)	16.6 (7.8) a	2.2 (1.8–2.6)	18.5 (17.0–20.6)
S77	91 (75.8%)	26 (21.6%)	3 (2.6%)	14.5 (7.3) b	2.1 (1.8–2.5)	16.5 (14.8–18.2)

* Groups with the same letter were not statistically different (Tukey test; $\alpha=0.05$).

according to the following scores: (a) adhesive (along the ceramic/cement interface); (b) cohesive with ceramics; (c) cohesive with cement; and (d) mixed (adhesive failure along the ceramic/cement failure interface+cohesive with resin).

2.8. Statistical analysis

Two statistical analyses were used to analyze the μ TBS results. One-way ANOVA and Tukey's test ($\alpha=0.05$), with the means of the repetitions (beams) from each block, were applied for treatment comparison. Weibull analysis with a Maximum Likelihood (MLD) model with a 95% confidence interval (CI) was used to compare the aged and non-aged groups [22]. The values of Weibull modulus (m) and characteristic strength (σ_0) were obtained to verify whether the aging process influences the bond strength survival of the groups. Only the bond strengths of specimens with adhesive failure were considered in the statistical analyses.

3. Results

The number of blocks and beams from each experimental group, the number and percentage of pre-test failures (PTF) during cutting and during aging, and the total number of beams tested are shown in Table 2. Among the groups, Group AS77 had the lowest PTF number during the cutting, followed by AS and S77. There was no PTF during the aging process. Tables 3 and 4 present the comparison between the non-aged and aged groups, respectively. Adhesive failure along the ceramic/cement interface was the predominant failure mode for all groups. This failure mode is shown in Figs. 1 and 2. AS and S77 had higher rates of cohesive failure than AS77, for both situations. The comparison of the μ TBS means of the adhesive failures showed no significant difference ($p=0.255$) for the non-aged groups (Table 3). The S77 group after aging was significantly inferior to AS77 and AS ($p=0.005$). As shown in Figs. 3–5, there was no difference in the Weibull modulus (m) and characteristic strength (σ_0) of the aged and non-aged specimens, for all comparisons. The similarity of the m values is indicated by the overlapping confidence intervals. The characteristic strength value of S77 (aged) was the lowest among the groups, and the m value of AS (nonaged) was the lowest.

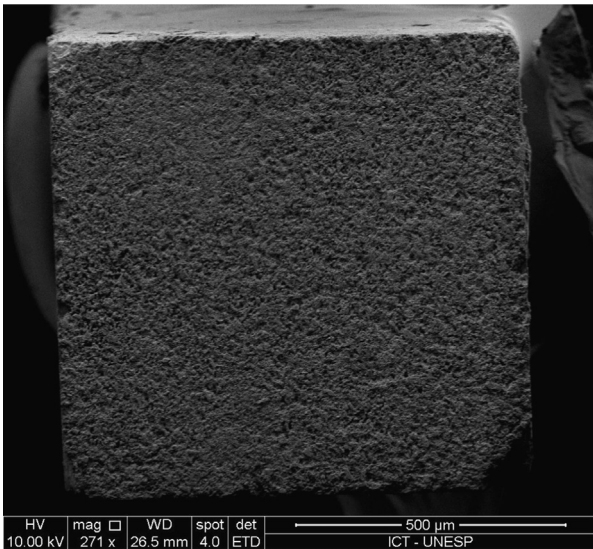


Fig. 1. SEM photomicrograph (ETD detector, 271 ×) of a ceramic slice from group AS77 with adhesive failure mode. This failure mode was predominant for all groups.

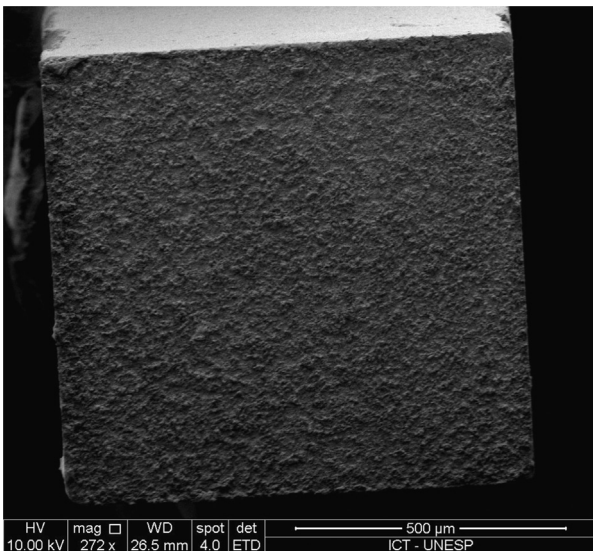


Fig. 2. SEM photomicrograph (ETD detector, 272 ×) of a resin slice from group AS77 with adhesive failure mode. This failure mode was predominant for all groups.

4. Discussion

Adhesion to silica-based ceramics has been studied and improved in recent years [5,6,8]. Although the conventional treatment involving hydrofluoric acid + silane provides acceptable bond strength between ceramic and resin cement [3,5], hazardous effects of the acid have led to studies to find alternative treatments for ceramic surfaces [3,5,6,8,12,17]. The findings of this study suggested that the three tested treatments, one excluding the hydrofluoric-acid-etching step, provided similar bond strengths to ceramic without aging by thermocycling. However, after the aging process, the results of the non-etched group were statistically lower compared with those of the etched groups, leading to partial rejection of the first study hypothesis.

Hydrofluoric acid etching of silica-based ceramics has the capacity of reacting with the glassy matrix to form a soluble hydrofluorosilic acid, which can be rinsed off. This reaction results in micromechanical retention on the surface and increases surface

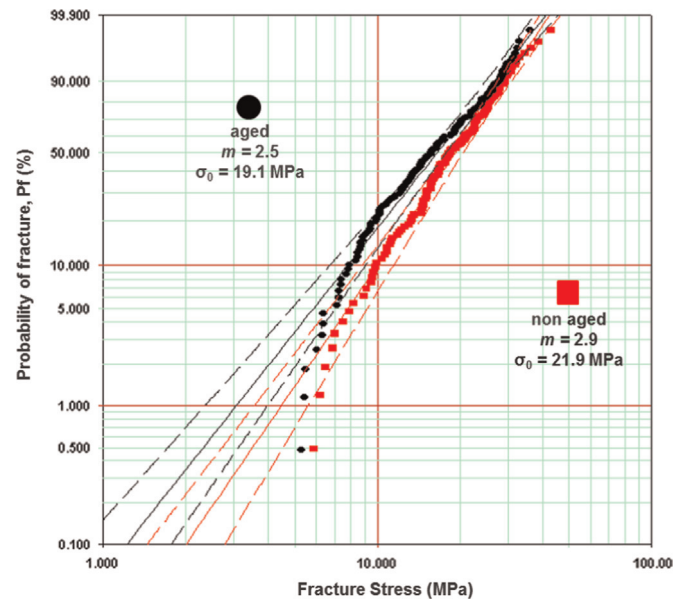


Fig. 3. Weibull comparison (Maximum Likelihood analysis – MLD) of the aged and non-aged AS77 groups.

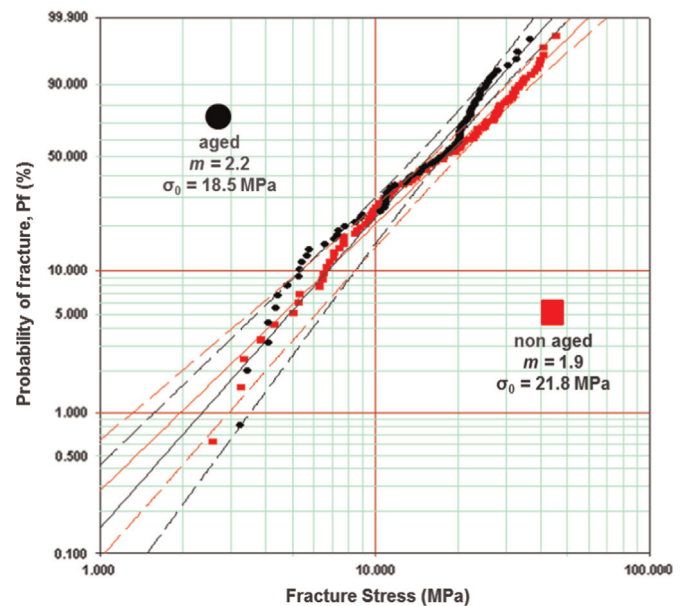


Fig. 4. Weibull comparison (Maximum Likelihood analysis – MLD) of the aged and non-aged AS groups.

energy [3]. Previous studies have reported higher bond strength of the ceramic–resin interface with HF rinsing compared with no rinsing [23] or even with sandblasting or surface-grinding [6]. The stability of the bond strength for the etched specimens in this study is in agreement with the results of a previous study [6] where the interface was not affected by 1-year storage. Moreover, the similarity between the m values of the aged and non-aged groups suggests that the reliability of the interface after HF etching was not affected by thermocycling.

Previous studies have shown the benefits of heat treatment for the bond strength between ceramic and cement [5,6,8,17]. The immediate bond strength values found in this study confirmed these findings, since the silanized + heated group (S77) promoted similar bond values to groups with hydrofluoric acid etching (AS and AS77). Although the heat treatment consisted of a warm air

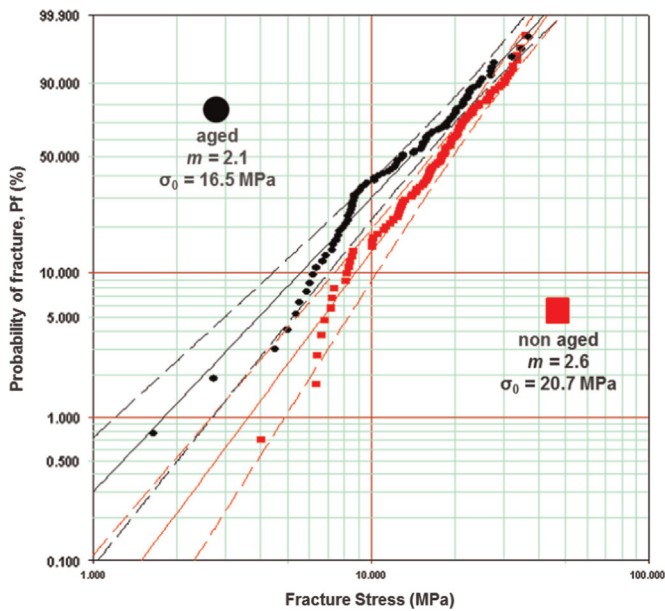


Fig. 5. Weibull comparison (Maximum Likelihood analysis – MLD) of the aged and non-aged S77 groups.

stream (100 °C) in some studies [5,6], in the present study, we attempted to isolate the temperature factor by using an oven. The heat treatment eliminated the silane by products and helped complete the reaction between silane and silica [8]. The association of the two treatments of this study (HF acid etching and heat) did not affect the μ TBS results. However, it did result in lower PTF rates during specimen sectioning, which suggests an improvement in the union between materials and can be used to optimize the clinical results during cementation.

A previous study by this research group [17] showed that heat treatment of the silane at 77 °C had a positive effect on interfacial bond strength, which was not affected by mechanical cycling (200,000 cycles). Once the previously selected mechanical fatigue regimen was found not to affect the bond strength of the system [17], the influence of this heat treatment was tested after thermocycling. The aim of this aging process was to induce some contraction/expansion stress at the interface as a result of the thermal coefficient differences of the materials [9] that could cause crack propagation among them. Although different thermocycling profiles have been reported in the literature [24–27], this study used 12,000 cycles. This protocol did not significantly affect the m and σ of the groups, but did reduce the mean values of the S77 group, which was significantly lower compared with the others. Moreover, the S77 group had the greater difference between the σ values compared (aged and non-aged), casting doubt concerning the long-term success of the treatments excluding acid etching. The similarity between the m of the groups suggests that aging did not affect the survival of the interfaces.

In contrast to previously reported literature reports [5,6,8,17], this study considered only the specimens with adhesive failure for statistical analyses, since pure adhesive failures express the actual situation of the tested interfaces. The high rate of pre-test failures during the cutting procedure is a limitation of this study, but it did not affect the statistical analysis, since the number of specimens tested was sufficient to find a difference between the aged groups.

Although producing significantly different results after thermocycling, HF use is still questionable, since the results were not markedly different from those in the group treated solely with silane and heated. Thus, clinical trials are necessary to show if there are clinically relevant differences between these protocols.

5. Conclusions

Heat treatment of silanized feldspathic ceramic (non-acid-etched surface) provided similar bond strength compared to the traditional hydrofluoric-acid-etching treatment before aging and lower bond strength after aging, partially rejecting the first hypothesis. The combination of the hydrofluoric-acid-etching and the heat treatment did not improve the bond strength, accepting the second study hypothesis. The thermocycling regimen selected for this study did not affect the reliability of the groups, accepting the third study hypothesis.

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