

A new silica-infiltrated Y-TZP obtained by the sol-gel method



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ABSTRACT

Objective: The aim of this study was to evaluate silica infiltration into dental zirconia (VITA In-Ceram 2000 YZ, Vita Zahnfabrik) and its effects on zirconia's surface characteristics, structural homogeneity and bonding to a resin cement.

Methods: Infiltration was performed by immersion of the pre-sintered zirconia specimens in silica sols for five days (ZIn). Negative (pure zirconia specimens, ZCon-) and positive controls (specimens kept in water for 5 days, ZCon+) were also performed. After sintering, the groups were evaluated by X-ray diffraction (XRD), grazing angle X-ray diffraction (DRXR), scanning electron microscopy (SEM), contact angle measurements, optical profilometry, biaxial flexural test and shear bonding test. Weibull analysis was used to determine the Weibull modulus (m) and characteristic strength (σ_0) of all groups.

Results: There were no major changes in strength for the infiltrated group, and homogeneity (m) was also increased. A layer of $ZrSiO_4$ was formed on the surface. The bond strength to resin cement was improved after zirconia infiltration, acid conditioning and the use of an MDP primer.

Conclusion: The sol-gel method is an efficient and simple method to increase the homogeneity of zirconia. Infiltration also improved bonding to resin cement.

Clinical significance: The performance of a zirconia infiltrated by silica gel improved in at least two ways: structural homogeneity and bonding to resin cement. The infiltration is simple to perform and can be easily managed in a prosthesis laboratory.

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1. Introduction

Dental ceramics are similar to the natural tooth in appearance because of their optical properties. This and other qualities, such as hardness [1] and chemical stability [2], enabled these materials to be rapidly developed for dental use, to meet the increasing demands for esthetics and durability.

The dental ceramics presenting better esthetics are silicates like feldspathic ceramic and lithium disilicate [3]. However, these ceramics have inferior mechanical properties compared with those

of zirconia. Thus, zirconia has been widely used as an infrastructure material in crowns and fixed partial prostheses, because of its excellent mechanical properties [4].

The remarkable performance of zirconia, as explored in various medical and engineering applications, is due mainly to the transformation of the tetragonal into the monoclinic phase. This transformation can be induced by thermomechanical factors, resulting in a volume increase of about 3–4%. This volume increase generates compressive stresses on the tip of a possible crack. In this case, for the crack to propagate, it must overcome the compressive stresses surrounding it. This toughening mechanism explains the high fracture resistance of zirconia when compared with that of other ceramics [5,6].

A common problem in zirconia is its difficulty in promoting adhesion compared with silica-based ceramics [7]. For feldspathic ceramics, conditioning the surface with hydrofluoric acid (HF 10%)

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is effective in creating mechanical imbrication, while silanization provides the chemical bond between the inorganic ceramic and the organic resin cement. However, for alumina- and zirconia-based ceramics HF is not able to roughen the surface sufficiently, and the absence of silica prevents chemical bonding to silanes [7]. Air abrasion with aluminum oxide alone, commonly performed in laboratories, also does not improve adhesion and creates micro-defects that compromise the strength of the material in the long term [8–10].

Until now, the preferred method for bonding zirconia is the combination of air abrasion with aluminum oxide particles coated with silica (silicatization) and the application of a phosphate-based monomer as an adhesion promoter. However, silicatization also has the potential to damage the surface [11–13].

Based on reports in the literature, the most frequent clinical failures of tooth- and implant-supported zirconia crowns are loss of retention and veneering material fracture [14]. To solve the retention problem, several methods were created to infuse silica into zirconia, making it chemically reactive to the bisphenol-A-glycidyl dimethacrylate (Bis-GMA)-based cements such as the PyrosilPen [15], the “glaze-on technique” [16,17], which uses a thin intermediate coating of acid-etchable glasses, and silica nano-coating [18]. Additional methods, such as selective glass infiltration [19] and a hot acidic solution [20] are intricate techniques that roughen zirconia and improve bonding. A new method for infiltrating pure silica in a Y-TZP using a sol-gel process was proposed in this present study to create a layer sensitive to acid etching and silanization.

By coating the Y-TZP we also aimed to produce a graded zirconia. This type of material presents increased load bearing capacity and a gradual increase in the elastic modulus towards the interior layers [21], which may improve the interfacial adhesion with porcelains [22].

Therefore, this first study aimed to evaluate the effects of such infiltration with a simple and low-cost sol-gel method on the mechanical properties, microstructure and surface characteristics of a Y-TZP. Additionally, we evaluated the bond strengths between the infiltrated ceramic and resin cement.

2. Materials and methods

2.1. Preparation of specimens

The pre-sintered zirconia blocks (Vita InCeram YZ, Vita Zahnfabrik, Bad Säckingen, Germany) were wet-ground into cylinders (18 mm in diameter) that were then sectioned into discs in a lathe (ISOMET 1000, Buehler, Lake Bluff, IL, USA). The first section (approximately 0.5 mm) was discarded, and the remaining sections (1.65 mm thickness) were cut under coolant irrigation. The discs were wet-ground flat with silicon carbide (SiC) (#1200) and sintered according to the manufacturer’s instructions (Vita Zyrcomat, Vita Zahnfabrik) according to the following schedule: temperature elevation time, 1 h; final temperature, 1530 °C; waiting time, 2 h; and cooling temperature at which the tray can be downloaded inside the oven, 400 °C. The final dimensions were according to ISO 6872 standard, being 12 mm in diameter and 1.2 mm thick.

The pre-sintered zirconia discs were divided into three groups. One group was immersed in water alone (Positive Control Group, ZCon+) and/or in silica sol (ZIn), both of which remained in these respective media for 5 d. The silica sol (0.5 mol/L) was obtained by passing an aqueous sodium silicate solution through an ion-exchanging resin. The third group was the negative control (ZCon-), which was not immersed in any medium. After the immersion period, the pre-sintered zirconia discs were removed from the

solution and put into an oven at 100 °C for two days. After being dried, the specimens were sintered in the same manner as the specimens of the non-infiltrated group.

The sintered specimens were then evaluated by X-rays, Raman spectroscopy, scanning electron microscopy (SEM), and contact angle measurements. X-ray diffraction (XRD) (X’pert Powder model, PANalytical, Westborough, MA, USA) was performed at 10–90°, with a scan step of 10.1600 s, at a 0.0170° step size, with CuK α radiation. The Rietveld refinement of the diffractometries was performed with the General Structure Analysis System (GSAS)/EXPGUI program (a graphical interface for the Los Alamos GSAS package). Raman spectroscopy was performed in a Micro Raman system (Renishaw 2000, Gloucestershire, UK) under Ar laser excitation, at a wavelength of 514.5 nm. The Raman spectra were collected over 3 accumulation periods of 30 s, between 200 and 3500 cm⁻¹. The contact angle analysis was performed in a tensiometer (Kruss, model EasyDrop DAS 100, Hamburg, Germany) Contact Angle Measuring Instrument using the sessile drop (Young-Laplace method) and distilled water (3 μ L).

2.2. Flexural strength, weibull parameters, and surface analyses

Thirty specimens were prepared for each group. Two outliers of the infiltrated zirconia were disregarded in the analysis and analyzed separately.

To determine flexural strength, we placed each disc on a circular base with three metallic beads of 3.2 mm in diameter, equidistant from each other, forming a plane. A blunt tip, 1.6 mm in diameter, was attached to a testing machine (EMIC DL-1000, EMIC, São José dos Pinhais, PR, Brazil), and a load was applied (1000 Kgf) until fracture at a constant speed of 1 mm/min.

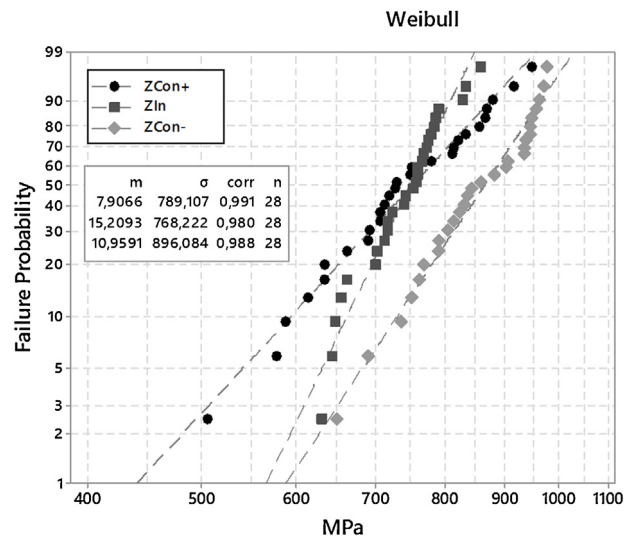


Fig. 1. Weibull plot of pure (ZCon-) zirconia, infiltrated zirconia (ZIn), and zirconia stored in water (ZCon+). The Weibull plot shows the steeper inclination of the line corresponding to the infiltrated group (higher Weibull modulus), with less dispersion of strength values than the positive and negative controls. The test for equal shape parameters ($P=0.001$) showed that the moduli of the negative and infiltrated groups were not significantly different, but were both superior to the modulus of the positive control group.

The biaxial flexural strength (σ) (MPa) of the discs was obtained according to the ISO 6872 standard:

$$\sigma = -0,2387P(X - Y)/b^2,$$

where: P =load (N); X and Y =are parameters related to a elastic property of the material [Poisson's ratio (0.3)] and the radii of the specimen and loading device (mm); and b =thickness of the specimen at the fracture origin in mm.

The Weibull parameters, modulus (Shape parameter) and characteristic strength (Scale parameter), were obtained from the Maximum Likelihood estimation (Minitab 16, Minitab Inc, State College, PA, USA) (Fig. 1).

Topographic and fracture analyses were performed by stereo-microscopy (Discovery V20, Carl Zeiss, Jena, Germany) and scanning electron microscopy (SEM) (Inspect S50, FEI Company, Brno, Czech Republic).

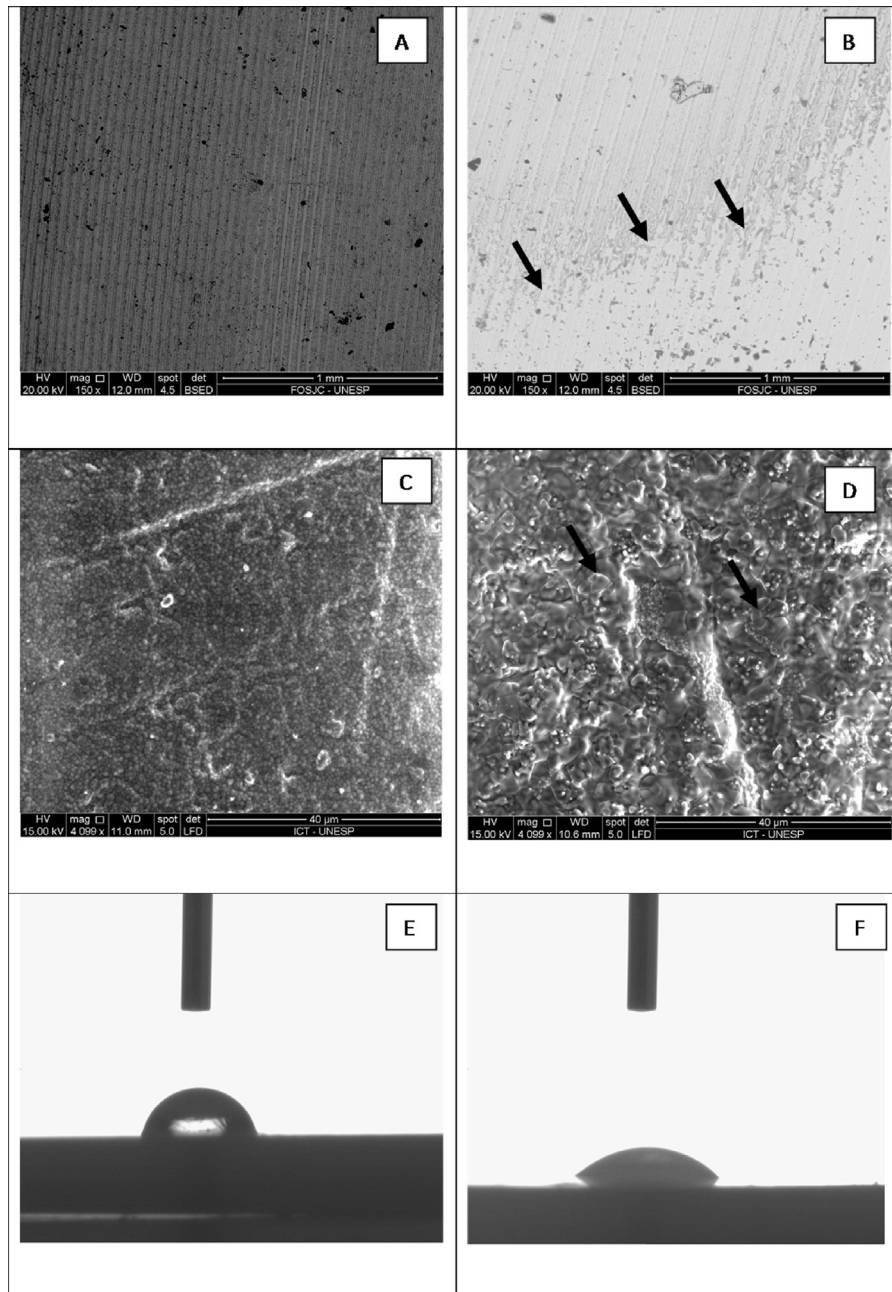


Fig. 2. Backscattered (A, B) and secondary (C, D) SEM and contact angle analysis of ZCon- (E) and ZIn (F) specimens. The charged areas indicate the deposition of silica, and the arrow indicates thicker deposition zones. In (C), one can see the zirconia grains, and in (D) the grains are permeated by the silica layer (arrows). The contact angles of pure (E) zirconia are higher than those of the infiltrated (F) specimens, in which the water is more spread.

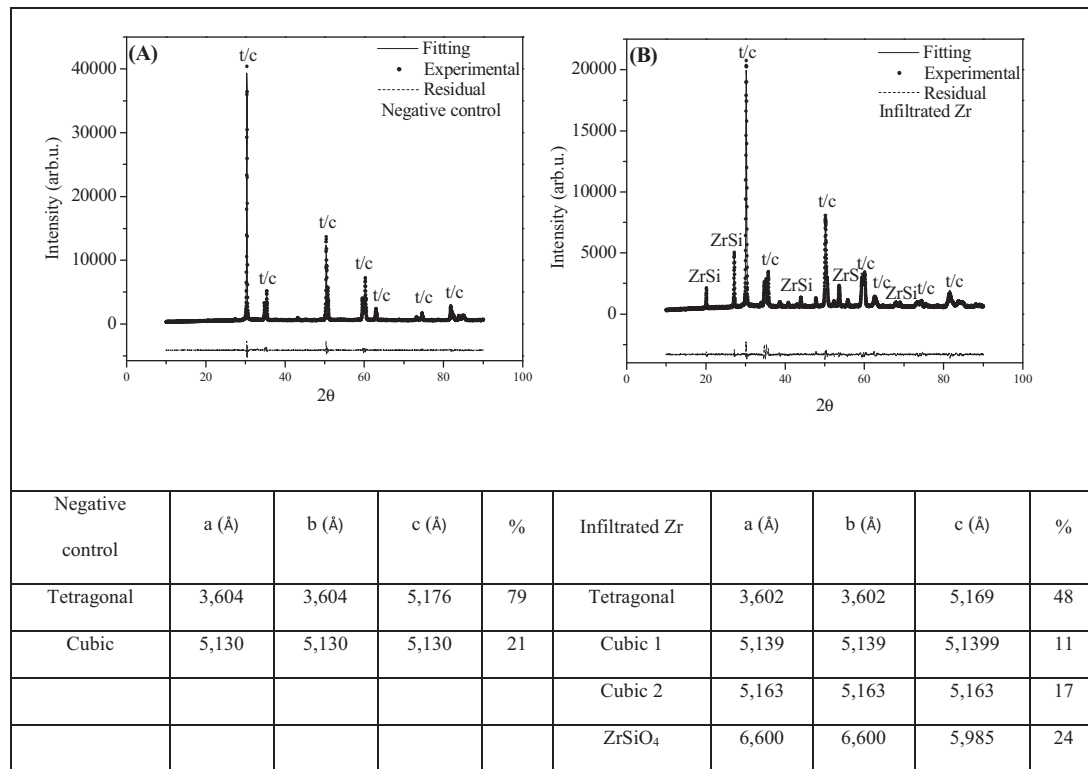


Fig. 3. X-ray diffractometries and curve-fitting of pure and infiltrated zirconia. Results of the Rietveld refinement show the percentages of phases and the lattice parameters (Å). The peaks signaled by t/c correspond to tetragonal and cubic phases, whereas the ZrSi correspond to the ZrSiO₄ composite.

A bond strength analysis was performed on square-shaped zirconia specimens. Specimens were divided in infiltrated and non-infiltrated groups (control). After sintering, the infiltrated groups were conditioned with 2% HF acid for 10 s. This acid concentration delivered the most favorable topography based on profilometry images of 2%, 5% and 10% of infiltrated specimens, after several exposition times (10 s and 15 s) (not shown here for brevity).

Specimens from both groups were then silanated with Monobond Plus or Monobond S (Ivoclar Vivadent, Schaan, Liechtenstein) and a resin cement cylinder (3 mm diameter and 6 mm height) (Variolink II, Ivoclar Vivadent, Schaan, Liechtenstein) was built up on each zirconia specimen. After photopolymerization for 40 s, specimens were stored in distilled water for 24 h at 37 °C. Half of them were then tested in shear in a universal testing machine, while the other half was further subjected to thermal cycling (5°–55 °C). After 6 × 10³ cycles, the specimens were tested in shear and all fractured surfaces were analyzed in a stereomicroscope to determine the failure modes.

3. Results

The lowest and highest Weibull moduli belonged to ZCon⁺ and ZIn groups, respectively (Fig. 1).

The silica infiltrated the bottom and top of the disc uniformly, but presented areas of increased deposition (Fig. 2A–D). The contact angles were inferior in the infiltrated specimens, which is a good indication of higher wettability and affinity to adhesive materials (Fig. 2E and F).

Fig. 3 shows that the infiltrated and negative control specimens presented peaks related to tetragonal and cubic zirconia; however, the former also presented peaks of zirconium silicate (ZrSiO₄). The specimens that were kept in water and the control group did not present phase changes; thus, only the infiltrated and the pure zirconia spectra are shown in Fig. 3. The Rietveld refinement identified the cubic and tetragonal phases, showing 79% of tetragonal and 21% of cubic phases.

Fig. 4 presents the fracture characteristics of all groups. The fracture origins were more prominent in the ZIn and ZCon⁻ groups than in ZCon⁺.

Fig. 5 presents the Raman spectra of control and infiltrated specimens in which the ZIn fractured specimen shows preserved capacity for phase transformation.

The bond strength analysis showed lower bonding values and greater scattering of the data of non-infiltrated groups (Fig. 7). Non-infiltrated specimens that did not receive a layer of MDP could not survive after thermal cycling (TC). Table 1 displays the results of the infiltrated groups. The infiltrated groups treated with MDP presented the highest bond strength values before thermal cycling. Profilometry images showed the topography varied according to the surface treatment (Fig. 6). All failures were adhesive at the bonding interface.

4. Discussion

The Weibull analysis showed that the homogeneity of the new material was superior, due possibly to healing of surface flaws. Leaching of zirconia kept in water probably caused a variation in

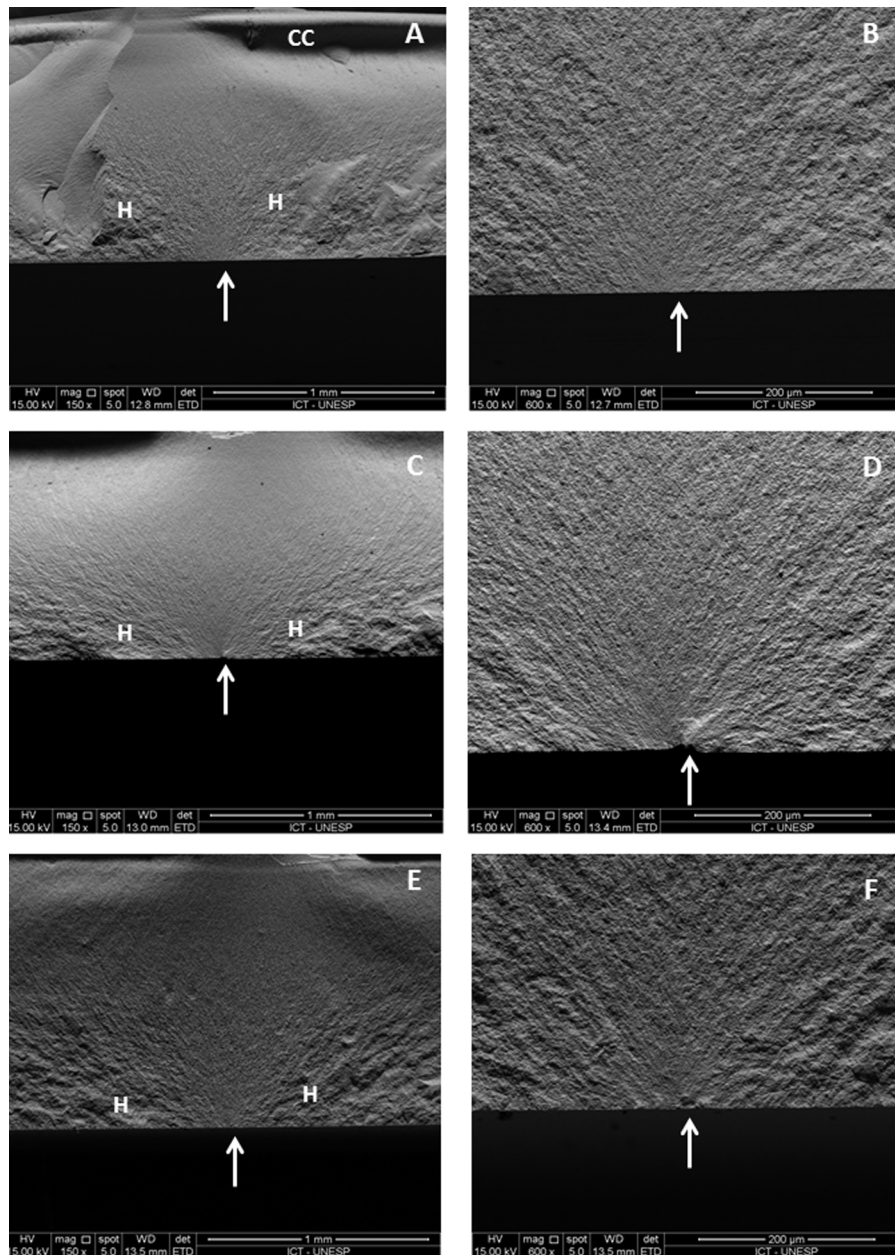


Fig. 4. SEM images of fractured specimens: ZCon+ (A and B), ZCon- (C and D) and ZIn (E and F). The white arrows indicate the failure origin in the bottom center of mirror regions. In A, several mist hackles (H) and a compression curl (CC) are seen. In C several hackles also irradiate from the origin. The origins are semi elliptical flaws, readily seen in D and F, whereas in B no defect can be defined.

the severity of the defects on the surface, leading to a low Weibull modulus. Thus, less energy must have been needed to fracture ZCon⁺ specimens.

The silica deposition also formed a sandwich of glass/zirconia/glass layers, which share the characteristics of the graded zirconia described by Zhang et al. [22]. This type of material presents a gradation of elastic moduli toward the interior of the zirconia, which increases its load-bearing capacity and protects against low thermal degradation.

The increase in the wettability of ZIn turns this material into a good substrate for bonding resinous materials, treatable with HF

and silanes. Moreover, the sol-gel infiltration presents the advantage of being a user-friendly method that does not impinge on the ceramic surface, as does air abrasion [23,24].

Silica infiltration was able to improve not only the immediate bond strength to resin cement, but also the long term bond strength after 6×10^3 thermal cycles. However, MDP primers have limited durability and that therefore explains the lower bond strengths between infiltrated zirconia and cement after thermocycling [12]. In spite of that, the bonding values were equivalent to the groups for which the infiltration was performed and no MDP was used, confirming that the

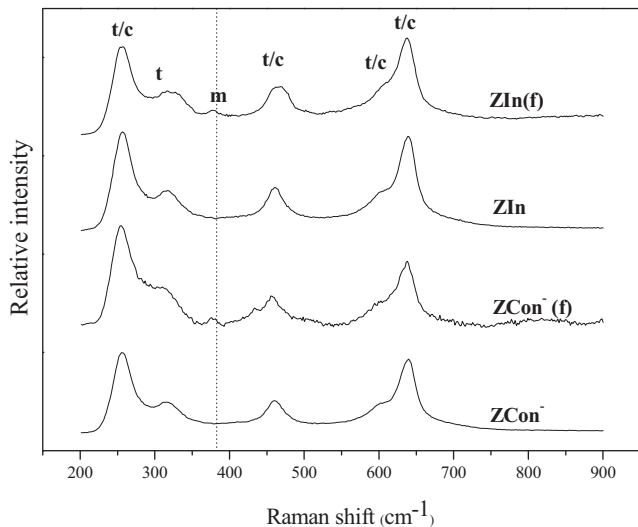


Fig. 5. Raman spectra of infiltrated and control zirconia of whole and fractured (f) specimens. Tetragonal zirconia (t), tetragonal and cubic zirconia, monoclinic zirconia (m).

mechanical interlocking is essential to preventing interfacial debonding.

The XRD peak analyses indicate that the silica diffused into the substrate and reacted with zirconia, forming an intermediate crystalline phase that tends to be more resistant to corrosion [25] because the pure silica gel infiltrated in the surface porosities is free of Sodium. But this needs further investigation.

It is important to highlight that the X-rays had limited penetration inside the material. Thus, heterogeneous materials, such as ceramic films, present peak intensities more representative of the film than the substrate. Because the Rietveld refinement is based upon the relative intensity of the peaks, the phase percentages are higher on the surface than in the bulk.

The infiltrated zirconia presented 24% of $ZrSiO_4$ and 48% tetragonal zirconia. The modified zirconia also presented two types of cubic zirconia, types 1 and 2, which corresponded to 11 and 17% of the material, respectively. Type 1 presents lattice parameters similar to those present in the control group; thus it can be said

Table 1

Bond strength data between zirconia and resin cement—Descriptive statistics [Mean, Standard Deviation (SD), and Coefficient of Variation (CV)] and Tukey's test of the infiltrated groups, with and without MDP and in the presence or in the absence of thermalcycling (TC). Different superscript letters mean statistically significant difference.

Infiltrated groups	n	Mean	SD	CV
MDP and TC	10	3.62 ^B	3.79	104.78
MDP no TC	10	11.64 ^A	5.31	45.63
No MDP and TC	10	3.80 ^B	9.71	255.29
No MDP no TC	10	3.31 ^B	2.67	80.80

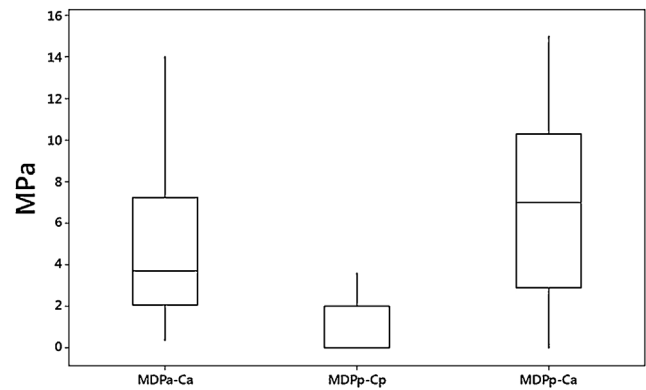


Fig. 6. Box-plots of the non-infiltrated groups, where a=absent; Ca=cycling absent; p=present; Cp=cycling present. After thermalcycling, the bond strengths were lower and presented greater variability than the initial bond strengths. The groups that did not receive an MDP coating did not survive thermalcycling and could not be tested.

that this cubic zirconia is the same type as present in the original substrate.

$ZrSiO_4$ and type 2 cubic zirconia are the main components of the film layer. This is possible because, at 1550 °C, silica on the zirconia surface can suffer a reaction on its solid state, resulting in zirconia silicate [26]. Besides $ZrSiO_4$, the formation of another type of cubic zirconia occurs concurrently, which can affect the final properties of the material. This means that phase transformation that makes zirconia tougher than other ceramics [27–30], which is manifested in the phase changing from tetragonal to monoclinic during mechanical stimuli [30], is not present in cubic zirconia [31]. The increase in cubic phase thus stabilizes zirconia.

The Raman spectra of intact and fractured infiltrated and control specimens presented the peaks related to tetragonal and cubic zirconia (250, 315, 460, 600, and 640 cm^{-1}) [30]. The only difference was the peak corresponding to monoclinic zirconia in the fractured specimens. Thus, one can suggest that the toughening transformation still occurs in the infiltrated zirconia and preserves its high toughness, but this needs more clarification. In spite of that, the mechanical properties of the infiltrated zirconia are slightly changed compared with those of pure zirconia, probably as a result of cubic phase formation.

The present study showed the sol-gel method was an efficient and simple way to increase the structural homogeneity and wettability of zirconia. Silica infiltration formed an intermediate crystalline phase and not only a juxtaposed silica layer. Additionally, the adhesion performance with 2% hydrofluoric acid for 5 s and MDP primer increased the bond strength to resin cement.

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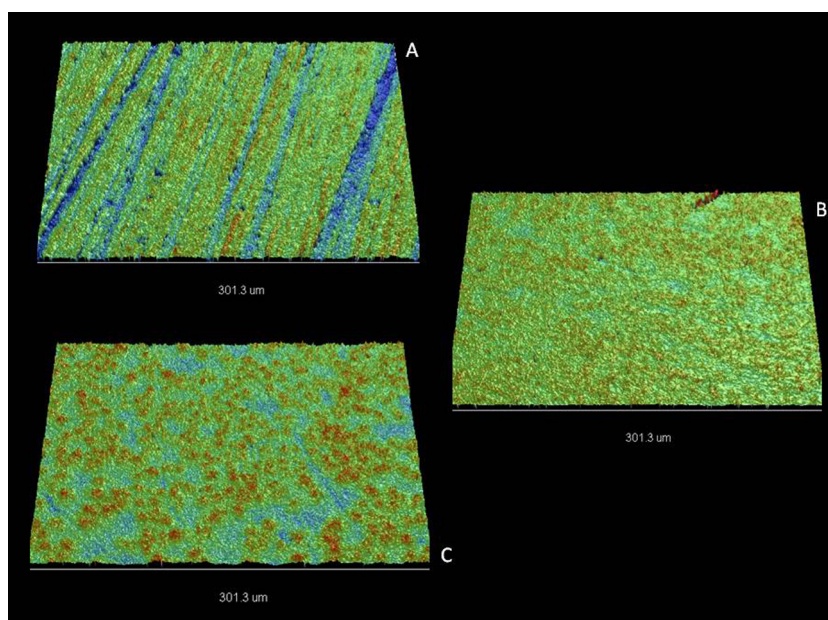


Fig. 7. Profilometry optical images of the zirconia surface untreated (A), infiltrated with silica without treatment (B) and infiltrated with silica and conditioned with HF 2% for 10 s (C).

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