



Kinetic parameters of red pepper waste as biomass to solid biofuel



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ABSTRACT

This work aimed to study the kinetic of thermal degradation of red pepper waste as solid biofuel to bioenergy production. The thermal degradation experiments were conducted at three heating rates, 5 °C/min, 7.5 °C/min and 10 °C/min in a thermogravimetric analyzer and oxidative atmosphere. The kinetic analysis was carried out applying the isoconversional model of Ozawa–Flynn–Wall. The activation energy was considerable low and varied 29.49–147.25 kJ/mol. The enthalpies revealed the energy difference between the reagent and the activated complex agreed with activation energies, the values of the pre-exponential factor indicated empirical first order reactions, Gibbs free energy varied from 71.77 kJ/mol to 207.03 kJ/mol and the changes of entropies had negative values, indicating that the degree of disorder of products formed through bond dissociations was lower than initial reactants. The calorific value was 19.5 MJ/kg, considered a relevant result for bioenergy production.

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1. Introduction

The agro-industry generates a large quantity the residues, also called biomass, which may be employed in the bioenergy generation. Several wastes are being used as biomass, including seeds, sewage sludge, leaves and algae (Santos et al., 2015b).

Worldwide data shows 1.3 billion of tons of food are wasted yearly which is equivalent to 750 billion dollars a year of damage (Food and Agriculture Organization, 2015).

Health-promoting, nutritional and sensory attributes make pepper as one of the most worldwide consumed vegetable (García, 2011) and *Capsicum sp.* powder is one of the most important spices. However, studies of the reuse and thermochemical properties of these residues have not been investigated (Santos et al., 2015b).

The red peppers cultivation has a greater importance and is considered the second most exported vegetable, encompassing

an annual worldwide production of 30 million tons in an acreage of 4 million ha (Freibauer et al., 2011).

The production of this fruit is considered one of the most important, representing the third in production and vegetable consumption, second only to garlic and onion (Milagres, 2014).

The quality and quantity of the obtained bioenergy depend not only on the chemical composition of original biomass but also on the reaction conditions. Thus, it is important to understand the chemistry of this alternative biomass in order to know the thermochemically conversion process into biomass-derived fuels (Lee et al., 2014).

This paper examines thermochemical red pepper waste conversion including thermodynamic parameters for non-isothermal analyses using Ozawa–Flynn–Wall (OFW) kinetic isoconversional model. Then the values of apparent activation energy (E_a), pre-exponential factor (A) in Arrhenius equation, as well as the changes of entropy (ΔS), enthalpy (ΔH) and free Gibbs energy (ΔG) were calculated. The calorific value was determined by calorimetric bomb.

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2. Methods

2.1. Sample preparation

The biomass of this study was the red pepper, *Capsicum baccatum* var. *pendulum*, waste. At the laboratory, the biomass was washed in tap water and dried naturally at room temperature for 24 h, followed by oven drying Solab model SL-100/42 at 105 °C to constant weight. The whole process lasted about seven days. After drying, the samples were ground in a Wiley mill, MA048 – Marconi, followed by sieving, Solutest sieve, NBR #200 (0.074 mm).

2.2. Thermal analysis

Thermogravimetric analysis were carried out at three different heating rates, 5°, 7.5° and 10 °C min⁻¹, using a simultaneous DSC-TGA equipment, TA Instruments, model SDT Q600, from 25 °C to 1000 °C. Air was used as purge gas at a 120 ml min⁻¹ flow rate. About (1.5 mg) of the biomass were used in alumina pans in each analysis. The TA Instruments software provides the thermogravimetry (TG) and derivative thermogravimetry (DTG) curves.

2.2.1. Calorific value

It was used a Calorimetric Bomb IKA C-200 and about 0.5 g was used for 10 min with 99.5% pure oxygen.

2.3. Kinetic study

As a matter of fact, the isoconversional analysis provides a fortunate compromise between the oversimplified but widely used single-step Arrhenius kinetic treatments and the prevalent occurrence of processes whose kinetics are multi-step (Vyazovkin and Sbirrazzuoli, 2006).

The one-step global model assumes that the degradation processes results in a single reaction, below.



k is defined as the rate constant of reaction whose temperature dependence is expressed by the Arrhenius equation

$$k = A e^{(-E_a/RT)} \quad (1)$$

where:

- E_a apparent activation energy (kJ/mol);
- T is the absolute temperature (K);
- R universal gas constant 8.31 J/K mol⁻¹;
- A is the pre-exponential factor (s⁻¹).

The rate of transformation from solid-state to volatile product is described by the following expression:

$$\frac{d\alpha}{dt} = k(T)f(\alpha) \quad (2)$$

where:

- A is conversion degree of the process;
- $k(T)$ is the time of process;
- $f(\alpha)$ is the rate constant and the reaction model.

Conversion, α , represent the normalized form of weight loss data of decomposed sample and is defined as below:

$$\alpha = \frac{m_i - m_\alpha}{m_i - m_f} \quad (3)$$

where:

- m_i is the initial mass of the sample;
- m_α is the actual mass;
- m_f is the mass after combustion.

Combining Eqs. (1) and (2) gives the fundamental expression (4) of analytical methods to calculate kinetic parameters, on the basis of TG results.

$$\frac{d\alpha}{dt} = A * f(\alpha) * e^{-E_a/RT} \quad (4)$$

The expression of the function $f(\alpha)$ and its derivative $f'(a)$ are used for describing solid-state first order reaction:

$$f(\alpha) = (1 - \alpha)^n \quad (5)$$

where:

n is the order reaction.

Substituting expression (5) into Eq. (4) gives the expression of reaction rate in the form:

$$\frac{d\alpha}{dt} = A * (1 - \alpha)^n * e^{E_a/RT} \quad (6)$$

For non-isothermal TG/DTG experiments at linear heating rate $\beta = dT/dt$, Eq. (6) can be written as:

$$\frac{d\alpha}{dt} = \frac{A}{\beta} * (1 - \alpha)^n * e^{-E_a/RT} \quad (7)$$

This equation expresses the fraction of material consumed in the time. In this work the activation energy was obtained from non-isothermal TG/DTG. The methods used to calculate kinetic parameters were non-isothermal and isoconversional Ozawa–Flynn–Wall methods and required tests at different heating rates.

2.3.1. Ozawa–Flynn–Wall methods

Kinetic analysis is essential to design and establish efficient, safe and reasonable processes. Determination of thermo-kinetic behavior of biomass allows control of decomposition mechanism of biomass. Kinetic parameters of reaction are necessary for accurately prediction of reactions behavior and optimization of the process towards products during thermal degradation (Ceylan and Topçu, 2014). Non-isothermal thermogravimetric analysis is the most popular and simplest method to study the kinetics and thermodynamics properties of biomass. An isoconversional integral method seems to be a safer alternative for the calculation of meaningful activation energy values for certain prerequisites, without knowing the kinetic model of the reaction mechanism.

The Ozawa–Flynn–Wall kinetics isoconversional method Eq. (8) was applied (Kim et al., 2010).

$$\ln(\beta) = C_\alpha - \frac{E_\alpha}{R \cdot T} \quad (8)$$

where:

- β heating rate;
- E_α apparent activation energy;
- C_α function of the conversion degree α ;
- R universal gas constant 8.31 J/K mol⁻¹;
- T the absolute temperature (K).

It was applied at least three values of heating rate (β) for different and same values of α in different absolute temperatures (T) in Kelvin (K) obtained at thermogravimetric curves. Allows to investigate whether the mechanism of the conversion is changing with the conversion degree, estimating the respective activation energy E_α at a conversion degree α . To calculate the kinetic parameters this work used an intermediate value of β (7.5 °C/min).

The thermodynamic parameters using OFW isoconversional method for analysis of kinetic studies and thermodynamic parameters including pre-exponential factor (A) in Arrhenius equation, as well as enthalpy (ΔH), free Gibbs energy (ΔG) and the changes of

entropy (ΔS) can be expressed by Eqs. (9)–(12) (Kim et al., 2010; Xu and Chen, 2013).

$$A = \beta \cdot E_a \exp\left(\frac{E_a}{R \cdot Tm}\right) / R \cdot Tm^2 \quad (9)$$

$$\Delta H = E_a - RT \quad (10)$$

$$\Delta G = E_a + R \cdot Tm \cdot \ln\left(\frac{K_B \cdot Tm}{h \cdot A}\right) \quad (11)$$

$$\Delta S = \frac{\Delta H - \Delta G}{Tm} \quad (12)$$

where:

K_B Boltzmann constant ($1.381 \cdot 10^{-23}$ J/K);

h Plank constant ($6.626 \cdot 10^{-34}$ J s);

Tm DTG peak temperature.

3. Results and discussion

3.1. Thermogravimetric analysis

Previous studies showed that biomass degradation can be divided into individual steps: water devolatilisation, hemicellulose, cellulose and lignin decomposition (Font et al., 2005). The decomposition of any biomass can be considered as the superposition of this main components (Manyà and Arauzo, 2008). This process is characterized by combustion of the residue formed, pyrolysis and oxidative pyrolysis (Conesa et al., 2014).

Thermal decomposition of lignin can occur in a temperature range from 180 °C to 900 °C, and mass loss rate is not as clear as in the case of hemicellulose and cellulose that decomposition has been estimated to be about 220–315 °C and 315–400 °C, with a maximum mass loss rate of about 268 °C and 355 °C (Gašparović, 2012).

The trends in weight loss curves obtained during the TG/DTG shows the physical and chemical structural changes occurring during the thermal conversion. Differential thermogravimetry (DTG) curve indicates main devolatilisation stages more clearly (Ceylan and Kazan, 2015). The curves have the typical appearance of degradation of lignocellulosic biomass just like the DTG curves obtained for the pyrolysis of cardoon leaves and stems at a heating rate of 10 °C/min (Xu and Chen, 2013) and the weight loss profile provided the instantaneous biomass weight at specific temperatures as biomass temperature was increased.

During the thermal degradation process up to 1000 °C with the heating rate of 5 °C/min, 7.5 °C/min and 10 °C/min, around 96.83 wt.%, 97.12 wt.% and 93.90 wt.% of the biomass can be volatilized, with a 3.17%, 2.87% and 6.09% of residual materials, respectively. The biochar formation was in a range of 200–440 °C and the ash contents displayed a positive correlation with degradation temperature (Xu and Chen, 2013). The presence of oxygen produces partial oxygenation of solid material, causing the apparent delay in the decomposition of the biomass.

This biomass allows producing biochar at lower temperature and biochar derived from herbaceous residues probably has distinct properties than that based on other plants (Lian et al., 2014).

Thermal analyses in the presence of oxygen, given the high exothermicity of the combustion reactions, a thermal decomposition may occur with the temperature inside the sample becoming considerably higher than that usual and the sample being oxidized at high reaction rate (di Blasi, 2009).

Fig. 1 demonstrates an example of a set of TG (A) and DTG (B) curves of DRP, obtained at 5 °C/min, 7.5 °C/min and 10 °C/min heating rates in air atmosphere. The thermal analysis data show

that the system is complex by the presence of overlapping reaction sequences and because of the complexity of the biomass samples of agricultural origin (CONESA; URUEÑA; DÍEZ, 2014).

Therefore, the thermal decomposition of volatiles materials and hydrocarbons at the biomass of DRP it was at about 200 °C as can see at Fig. 1 (step 1) (Ceylan and Kazan, 2015). This stage it was followed by thermal decomposition what means that the biomass has thermal stability (Turmanova et al., 2008), followed by a major loss of mass in the temperature range of 200 and 370 °C releasing the volatiles organics, characterizing the devolatilisation processes (step 2) (Damartzis et al., 2011).

The step 3 about 350 °C shows thermal degradation of DRP of some carbohydrates such as cellulose and others and the step 4 its associated at thermal decomposition of cellulose and lignin at about 400 °C (Damartzis et al., 2011; Sasmal et al., 2013). The lignin decomposition begins at the below temperatures and up to 550 °C. This high temperature is associated with the thermal stability and is responsible for the biomass degradation and residues during the decomposition process (Burhenne et al., 2013).

The presence of lowest cellulose content contributes to the less crystalline structure and recalcitrant characteristics of the material. The decomposition of biomass with high lignin content presents endothermic reaction, whereas decomposition of herbaceous biomass, with lower lignin content, involves an exothermic reaction (Yang et al., 2006).

The correlation between biomass and the cellulose, hemicellulose and lignin fractions was not very accurate (Couhert et al., 2009). Nevertheless, since the components differ significantly in their decomposition behavior, it is possible to determine clear trends in decomposition time, reaction enthalpy and composition of any biomass according to its composition of lignin, cellulose and hemicellulose (Ranzi et al., 2008). After step 4 occurs oxide formation.

In the temperature range of 200 °C and 500 °C it was a thermal decomposition of flavonoid and phenolic presents at capsaicinoids, as well fatty acids, (i.e. Linoleic, Oleic and Palmitic acids) and they become typical products of lignin decomposition.

3.2. Kinetic studies

The kinetic of thermal decomposition of biomass is an important component in the efficient design of thermochemical processes for the conversion of biomass (Turmanova et al., 2008). These processes have mechanisms very often unknown or too complex to be characterized by a simple kinetic model. They tend to occur in multiple steps that have different rates and to describe their kinetics, isoconversional methods are often used (Vyazovkin and Sbirrazzuoli, 2006).

The superposition of the decomposition of the single components it was used to predict thermal and kinetic behavior of biomass from its composition simply (Burhenne et al., 2013).

The Fig. 2 represents the curves of conversion degree vs. temperature at different heating rates, 5 °C/min (A), 7.5 °C/min (B) and 10 °C/min (C) in air atmosphere and the prediction does exhibits a good agreement with experimental data. Thanks to these results, the conversion degree and mass loss values can be used in order to better understand the biomass behaviors.

Two different stages can be observed in the process and they characterize a heterogeneous process and the lower heating rate, lower is the temperature at which they occur (Salla et al., 2003). The first stage, at lower temperature, in the temperature range 450–575 K is associated with thermal degradation of the biopolymers (i.e. cellulose) and the second at temperature 575 K, with degradation of the carbonaceous matter formed in the first stage (Leroy et al., 2010; Salla et al., 2003).

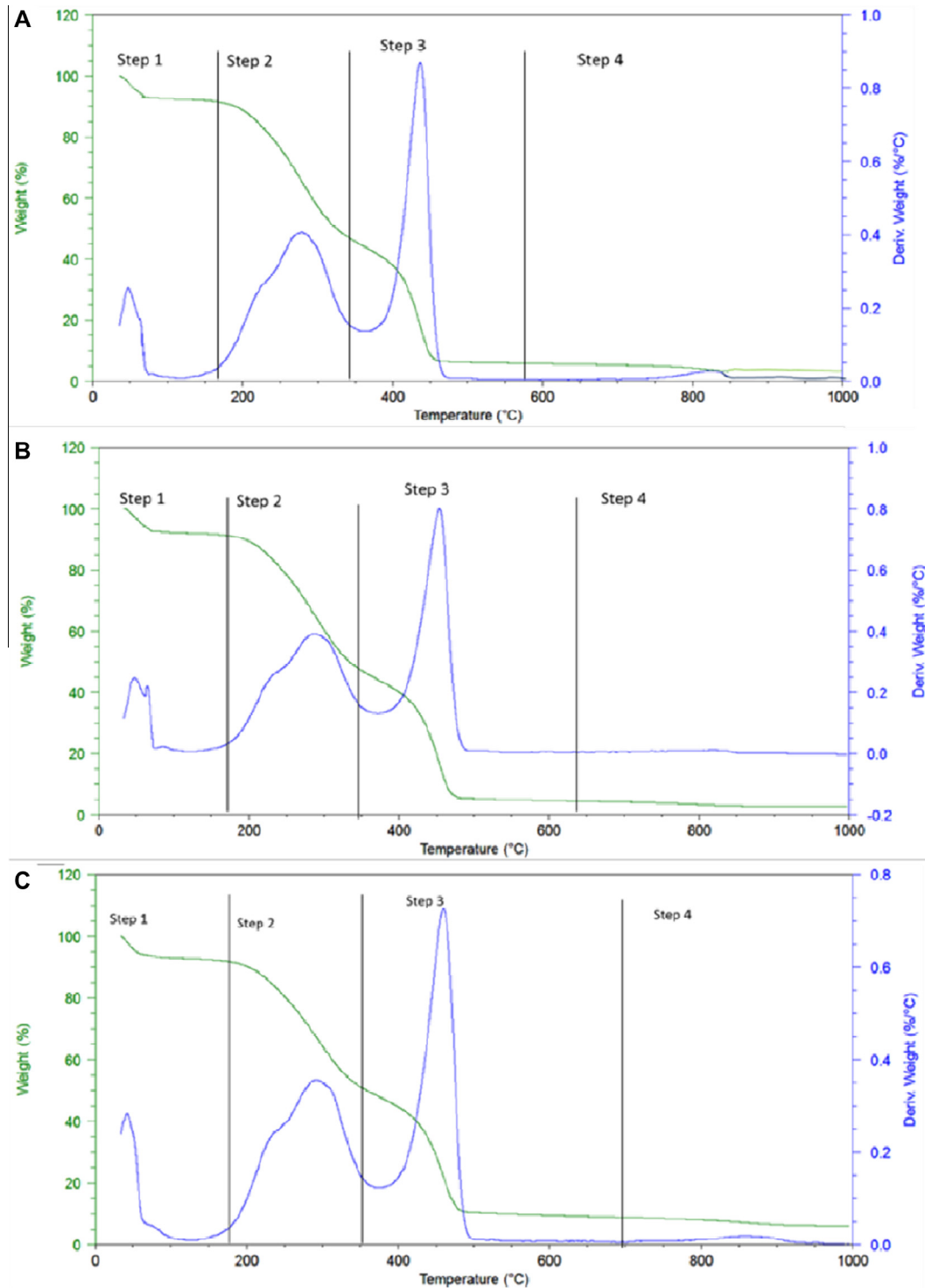


Fig. 1. Devolatilisation stages of RPW with heating rate of 5 °C/min (A), 7.5 °C/min (B) and 10 °C/min (C) in air atmosphere.

Data from TG and DTG curves in the decomposition range $0.1 < \alpha < 0.9$ were used to determine the kinetic parameters of the process in all used calculation procedures. The Fig. 3 represents $\ln \beta$ versus $\alpha (1/T)$ using TG curves presents in Fig. 1. During the thermal degradation of this biomass the energy barrier has to be overcome and can be observed that at the initial process, before the thermal process, all of bonds are not modified.

The estimate of the activation energy released chemical reactions complicated by physical transformations of biomass, the chemical stability of a compound is directly proportional to the value of activation energy.

Therefore, to ensure the decomposition of the stable molecules presents in that biomass, it is necessary to supply more energy, because is already know that during the decomposition of these

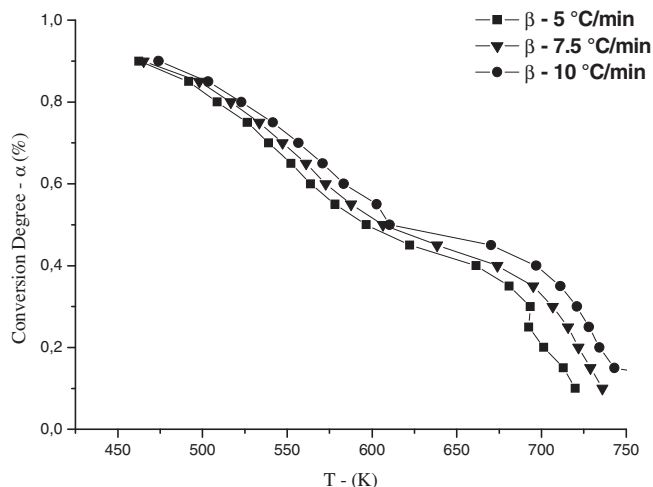


Fig. 2. Curves of conversion degree vs. temperature at different heating rates.

stable molecules at high temperature, less stable molecules which are easier to decompose are formed resulting in the lowering of heat supply.

It is already known that there are molecules easier to decompose and they are formed at higher temperature and the value of the activation energy decreases with the increase of conversion processes.

The apparent activation energy varied with increasing conversions and that shows volatiles degradation about α 50–85% (Manikandan et al., 2012). Thus, the DRP biomass presents two small values of activation energy in the range α 10 and 45% between 29.49 kJ/mol and 47.83 kJ/mol. The variation of values of activation energies are not similar at different constant extents of conversion because most solid-state reactions are not simple one-step mechanism and follow a complex multi-step reaction (Heydari et al., 2015).

According (Markovska et al., 2010), values of the activating energy found on the range of 60–120 kJ/mol are comparatively low. These values indicate that higher activation energy is only needed to decompose biomass with higher lignin content (Burhenne et al., 2013).

In lignocellulosic biomass the activation energy can vary from 80 kJ/mol to 200 kJ/mol to hemicellulose, 195–286 kJ/mol to cellu-

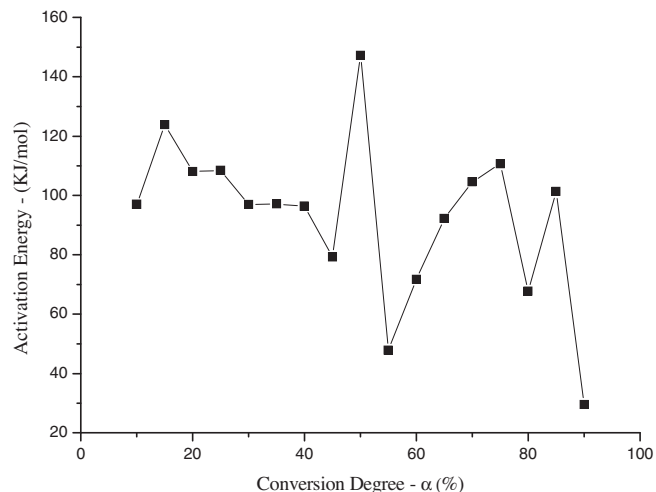


Fig. 4. Changes of Activation Energy during the biomass degradation process.

lose and 18–65 kJ/mol to lignin. The apparent activation energies of RPW varied from 29.49 kJ/mol to 147.25 kJ/mol. Olive residue and sugar cane bagasse have a value of 153–162 kJ/mol and 168–180 kJ/mol, respectively, due to the hemicellulose degradation, rice straw have a 166.98 kJ/mol and rice bran 115.124 kJ/mol (Xu and Chen, 2013).

The initial activation energy value was considered low due to cleavage of some weak bonds and elimination of volatile components from the biomass because at the beginning of the process all the strong bonds are not cleaved (Gašparovič, 2012; Markovska et al., 2010).

It was also observed decreasing dependences when studying the thermal degradation of biomass and interpreted this fact as the transition of the process in air atmosphere (Leroy et al., 2010).

The Fig. 4 represents the values of E_{α} during the process. The changes of enthalpies revealed the energy difference between the reagent and the activated complex agreed with activation energies (Dweck, 2008). The variation of enthalpy as well as respective activation energy changes represents the residual carbonaceous material (Turmanova et al., 2008). The change of activation enthalpy also shows the energy differences between the activated complex and the reagents. If this difference is small, the formation of acti-

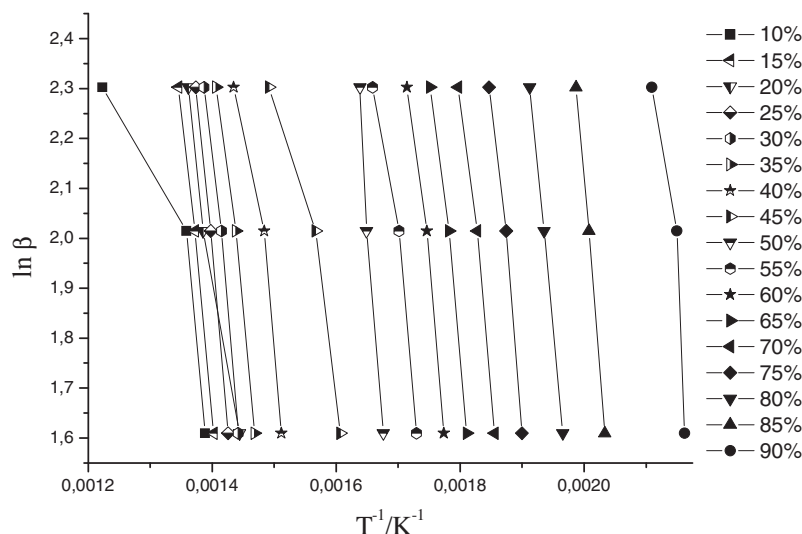


Fig. 3. Ozawa-Flynn-Wall isoconversion method applied to the thermal processing TG data of RPW in open pans within 10–90% of conversion.

Table 1
Kinetic Parameters of RPW with heating rate of 5 °C/min (A), 7.5 °C/min (B) e 10 °C/min (C) in air atmosphere.

Conversion degree (α)	E_a (kJ/mol)	A (s^{-1})	ΔH (kJ/mol)	ΔG (kJ/mol)	ΔS (J/mol)
10%	29.49	3.80E+00	23.37	207.03	-249.52
15%	101.33	1.98E+06	95.27	198.08	-141.03
20%	67.73	5.86E+03	61.73	197.70	-188.37
25%	110.67	1.47E+07	104.73	192.92	-123.24
30%	104.51	6.30E+06	98.64	138.59	-56.52
35%	92.17	9.10E+05	86.39	112.16	-37.06
40%	71.77	3.28E+04	66.17	71.77	-8.31
45%	47.83	5.44E+02	42.53	104.89	-97.69
50%	147.25	1.11E+12	142.21	159.51	-28.53
55%	79.31	1.46E+06	74.42	157.38	-141.14
60%	96.35	1.03E+08	91.60	151.85	-105.23
65%	97.16	1.95E+08	92.50	148.47	-99.76
70%	96.93	3.30E+08	92.38	144.46	-95.17
75%	108.48	9.04E+09	104.04	140.03	-67.44
80%	107.99	1.90E+10	103.69	136.24	-62.98
85%	123.88	2.80E+12	119.74	129.30	-19.20
90%	97.04	2.01E+10	93.17	105.49	-26.49

vated complex is favored, because the potential energy barrier is low (Vlaev et al., 2007).

The enthalpy variation of RPW was between 23.37 kJ/mol and 142.21 kJ/mol and it was already determined that rice bran have 111.03 kJ/mol of ΔH , rice straw have 162.23 kJ/mol and chicken manure presents 165.45 kJ/mol (Xu and Chen, 2013).

3.3. Thermodynamic parameters

The Table 1 shows the kinetic parameters at the point of maximum conversion. The pre-exponential factor values for solid phase reactions are expected to be in range 10^6 and 10^7 and are directly related with material structure while the reactivity of samples is determined by the activation energy (Vlaev et al., 2007).

The value ranged from 10^4 to $10^{18} s^{-1}$ showed empirical first order pre-exponential factors. The parameter showed variations to conversion rates. This may be described to the complex composition of the samples and the complex reactions that occur during decomposition (Turmanova et al., 2008).

The low pre-exponential factors ($<10^9 s^{-1}$) may indicate mainly a surface reaction, but if the reactions are not dependent on surface area, the low factor may indicate a closed complex. The high factors indicate a simple complex ($\geq 10^9 s^{-1}$) (Turmanova et al., 2008). The values of A between 10^{10} and $10^{12} s^{-1}$ reveals the activated complex was probably restricted in rotation compared to the initial reagent (Xu and Chen, 2013).

The value of pre-exponential factor less than 10^4 shows lower activation energy values, in this case 29.49 kJ/mol and 67.73 kJ/mol and represents the degradation of hemicellulose which occurs in steps 1 and 2. These lower values in A and E_a indicate a faster and easier degradation effect of this biomass for the respective degrees of conversion (Santos et al., 2015a).

The values showed in this study presents all range above, showing that the biomass studied is complex, as well all the phases of degradation can occur during the reaction. The range of pre-exponential factor for RPW was from 3.80E+00 to 2.80E+12. Rice straw presents values of pre-exponential factor between 1.70E+07 and 9.35E+12, rice bran presents 1.00E+07 and 1.58E+10 and chicken manure presents values between 1.00E+07 and 1.27E+13 (Xu and Chen, 2013).

The lower value of the apparent activation energy and pre-exponential factors of thermal degradation of biomass was due to the significant amount of porous carbon. This porous carbon easily burns in oxidative atmosphere and facilitates the thermal degradation of the red pepper waste (Turmanova et al., 2008).

Changes of entropies showed in Table 1 had negative values, indicating that the degree of disorder of products formed through bond dissociations was lower than that of initial reactants. The ΔS from RPW varied from -8.31 J/mol to -249.52 J/mol and showed higher values than rice straw and rice bran, -4.13 J/mol and -62.14 J/mol, respectively.

Low activation entropy meant that the material has just passed through some kind of physical or chemical aging process, bringing it to a state near its own thermodynamic equilibrium. In this situation, the material shows little reactivity, increasing the time taken to form the activated complex. On the other hand, when high activation entropy values are observed, the material is far from its own thermodynamic equilibrium. In this case, the reactivity is high and the system can react faster to produce the activated complex, which resulted in the short reaction times observed (Turmanova et al., 2008).

The changes of the Gibbs free energy showed the total energy increase of the system at the approach of the reagents and the formation of the activated complex (Kim et al., 2010; Sheng et al., 2014; Turmanova et al., 2008). The Gibbs free energy varied from 71.77 kJ/mol and 207.03 kJ/mol from RPW. The same parameters showed to rice straw 164.59 kJ/mol, rice bran 167.17 kJ/mol and chicken manure 175.29 kJ/mol (Xu and Chen, 2013).

The biomass calorific value estimated was 19.5 MJ/kg and this value is very similar with calorific values calculated for wood, 19.1 MJ/kg, Lignite chars 20.8 MJ/kg, coal 28.2 MJ/kg, Palm olive kernel 20.4 MJ/kg, Forest residue 21.7 MJ/kg and Cotton residue 18.3 MJ/kg, according (Kastanaki and Vamvuka, 2006).

4. Conclusions

The potential use of red pepper waste as solid biofuel was appropriated and this product could be used in the industrial processes, favoring an agro-industry based competitive world economy. It was found that the presence of oxygen increased the value of the apparent E_a and decreased the peak temperature and the activation energies calculated from the TG had the highest values in the order of 147.25 kJ/mol. The variation of apparent E_a represent a multi-step kinetics on the degradation process The A shows a first order reaction varying from 3.28E+04 s^{-1} to 2.80E+12 s^{-1} . The ΔS varied from -8.31 J/mol to -249.52 J/mol showed that the biomass has a high degree of arrangement and had physical and/or chemical process. The energy content of biomass was 19.5 MJ/kg. The OFW model is in good accordance with the exper-

imental data and satisfactorily described the complexity of degradation process.

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