

RESSALVA

Atendendo a solicitação do autor, o texto completo desta tese será disponibilizado somente a partir de 20/05/2023.



SÃO PAULO STATE UNIVERSITY (UNESP)
“JÚLIO DE MESQUITA FILHO”
SCHOOL OF ENGINEERING
ILHA SOLTEIRA - SP

MARCO ANTONIO LEITE BETETO

H_∞ AND *H₂* GAIN SCHEDULING STATE DERIVATIVE FEEDBACK CONTROL
BASED ON LMIs FOR LINEAR PARAMETER-VARYING SYSTEMS

Ilha Solteira
2022

A decorative graphic in the bottom right corner of the page, consisting of overlapping geometric shapes (triangles and squares) filled with a light blue dotted pattern, creating a modern, abstract design.

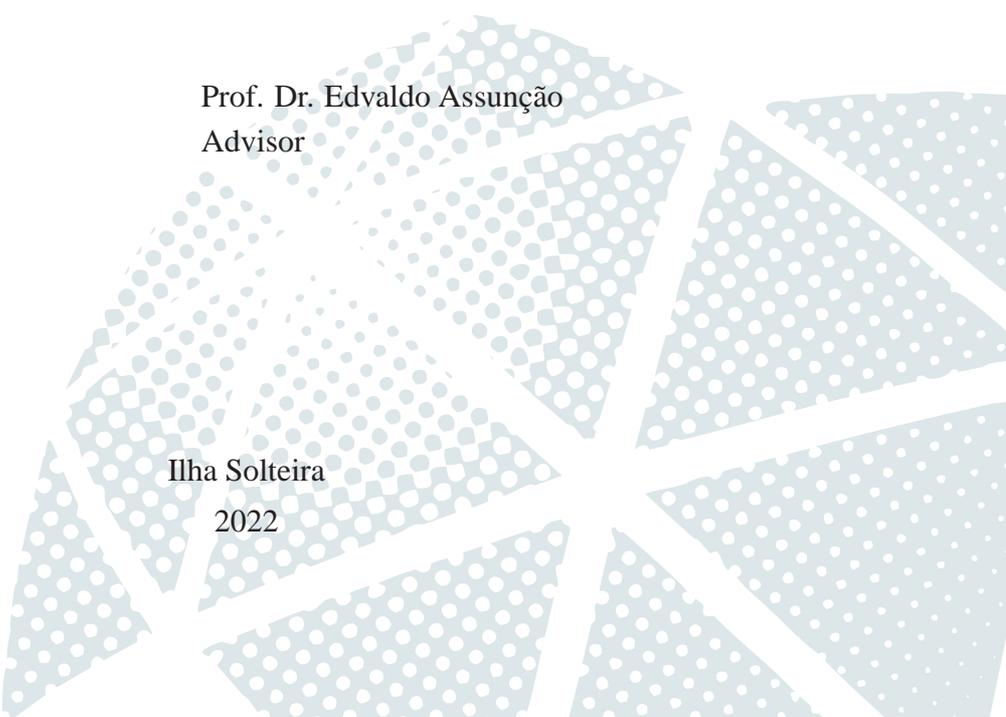
MARCO ANTONIO LEITE BETETO

**\mathcal{H}_∞ AND \mathcal{H}_2 GAIN SCHEDULING STATE DERIVATIVE FEEDBACK CONTROL
BASED ON LMIs FOR LINEAR PARAMETER-VARYING SYSTEMS**

Thesis presented to the São Paulo State University (UNESP) - School of Engineering - Campus of Ilha Solteira, in fulfilment of one of the requirements for the degree of Doctor of Science in Electrical Engineering.
Speciality: Automation.

Prof. Dr. Edvaldo Assunção
Advisor

Ilha Solteira
2022



FICHA CATALOGRÁFICA

Desenvolvido pelo Serviço Técnico de Biblioteca e Documentação

B562h Beteto, Marco Antonio Leite.
Hoo and H2 gain scheduling state derivative feedback control based on LMIs for linear parameter-varying systems / Marco Antonio Leite Beteto. -- Ilha Solteira: [s.n.], 2022
128 f. : il.

Tese (doutorado) - Universidade Estadual Paulista. Faculdade de Engenharia de Ilha Solteira. Área de conhecimento: Automação, 2022

Orientador: Edvaldo Assunção
Inclui bibliografia

1. Desigualdades Matriciais Lineares (LMIs). 2. Gain Scheduling (GS). 3. Realimentação derivativa. 4. Custo garantido Hoo. 5. Custo garantido H2. 6. D-estabilidade.

Raiane da Silva Santos
Raiane da Silva Santos

CERTIFICADO DE APROVAÇÃO

TÍTULO DA TESE: Hoo and H2 Gain Scheduling State Derivative Feedback Control Based on LMIs for Linear Parameter-Varying Systems.

AUTOR: MARCO ANTONIO LEITE BETETO

ORIENTADOR: EDVALDO ASSUNÇÃO

Aprovado como parte das exigências para obtenção do Título de Doutor em ENGENHARIA ELÉTRICA, área: Automação pela Comissão Examinadora:

A handwritten signature in blue ink, appearing to read "Edvaldo Assunção".

Prof. Dr. EDVALDO ASSUNÇÃO (Participação Virtual)
Departamento de Engenharia Elétrica / Faculdade de Engenharia de Ilha Solteira - UNESP

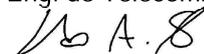
A handwritten signature in blue ink, appearing to read "Marcelo Carvalho Minhoto Teixeira".

Prof. Dr. MARCELO CARVALHO MINHOTO TEIXEIRA (Participação Virtual)
Departamento de Engenharia Elétrica / Faculdade de Engenharia de Ilha Solteira - UNESP

Prof. Dr. RODRIGO CARDIM (Participação Virtual)
Departamento de Engenharia Elétrica / Faculdade de Engenharia de Ilha Solteira - UNESP

A handwritten signature in blue ink, appearing to read "Bruno Augusto Angélico".

Prof. Dr. BRUNO AUGUSTO ANGÉLICO (Participação Virtual)
Depto. de Eng. de Telecomunicações e Controle / Escola Politécnica da USP

A handwritten signature in blue ink, appearing to read "Leonardo Ataíde Carniato".

Prof. Dr. LEONARDO ATAÍDE CARNIATO (Participação Virtual)
Departamento de Indústria / Instituto Federal de Educação, Ciência e Tecnologia de São Paulo (IFSP), Câmpus Presidente Epitácio.

Ilha Solteira, 20 de maio de 2022

*I dedicate this work to my parents, Luciana and Claudemir;
To my sister Emanuela;
To my girlfriend Ana Paula;
for all love, support, trust and encouragement at all times.*

ACKNOWLEDGEMENTS

My thanks to all the relatives, friends, professors and employees of FEIS-UNESP, who directly or indirectly contributed to the accomplishment of this work. In particular, I give my thanks:

- To God, for giving me strength and health to get here;
- To my relatives, especially my parents, my sister and my girlfriend, present at all times;
- To my advisor, Dr Edvaldo Assunção, for the friendship, the teachings, the patience and, mainly for the opportunity, incentive and confidence;
- To Professor Dr Marcelo Carvalho Minhoto Teixeira, for the friendship, suggestions and conversations, besides all the help and contributions for this work;
- To Dr Rodrigo Cardim, for the follow-up in the examining boards, suggestions and incentive;
- To the friends of the Research Laboratory in Control (LPC), Bruno Sereni, Leonardo Carniato, Gilberto, Douglas, Lázaro, Adalberto, Leidy, Hadamez, Marco, Gustavo, for the friendship and the contribution, that directly or indirectly helped;
- To the fomentation agencies, once that this study was financed in part by the Coordenação de Aperfeiçoamento de Pessoal de Nível Superior - Brasil (CAPES) - Finance Code 001, and Conselho Nacional de Desenvolvimento Científico e Tecnológico (CNPq);
- To the Foundation for Research Support of the State of São Paulo - FAPESP (Case number 2011 / 17610-0)

"Nothing in this world can take the place of persistence. Talent will not; nothing is more common than unsuccessful men with talent. Genius will not; unrewarded genius is almost a proverb. Education will not; the world is full of educated derelicts. Persistence and determination alone are omnipotent. The slogan Press On! has solved and always will solve the problems of the human race."

Calvin Coolidge (1872 - 1933)

"The beginning of a habit is like an invisible thread, but every time we repeat the act we strengthen the strand, add to it another filament, until it becomes a great cable and binds us irrevocably thought and act."

Orison Swett Marden (1848 - 1924)

RESUMO

Neste trabalho, são propostas novas condições para o controle de sistemas lineares dependentes de parâmetros variantes no tempo (do inglês, *Linear Parameter-Varying* - LPV), considerando a realimentação derivativa. A princípio, será abordado o problema \mathcal{H}_∞ para então obter condições para o controlador de realimentação derivativa *gain scheduling* \mathcal{H}_∞ . Em seguida, condições para o controlador de realimentação derivativa *gain scheduling* \mathcal{H}_2 são obtidas. O projeto dos controladores é baseado em desigualdades matriciais lineares (do inglês, *Linear Matrix Inequalities* - LMIs). É importante ressaltar que será considerada também a \mathcal{D} -estabilidade no projeto de controle, como forma de obter bom desempenho com um sinal de controle passível de implementação em um sistema real. Aqui, as condições para a \mathcal{D} -estabilidade serão tratadas no sentido de sistemas invariantes no tempo, com valores fixos do parâmetro variante em seu intervalo de variação. Ademais, as condições propostas levam em conta uma função de Lyapunov quadrática comum (do inglês, *Common Quadratic Lyapunov Function* - CQLF) para, em seguida, serem comparadas com as condições propostas considerando uma função de Lyapunov dependente do parâmetro variante (do inglês, *Parameter-Dependent Lyapunov Function* - PDLF). Este trabalho também oferece condições necessárias e suficientes para o controle misto $\mathcal{H}_\infty/\mathcal{H}_2$, ou seja, junta ambos, o problema \mathcal{H}_∞ e o problema \mathcal{H}_2 . As condições propostas são aplicadas em diversos exemplos para mostrar que utilizando-as é possível diminuir o custo garantido \mathcal{H}_∞ e \mathcal{H}_2 , ou seja, minimizar o efeito de um possível distúrbio no sistema. Além disso, por meio de um sistema instável, tem-se que com as condições propostas pode-se ao mesmo tempo estabilizar o sistema e minimizar o custo garantido.

Palavras-chave: Desigualdades Lineares Matriciais (LMIs). *Gain Scheduling* (GS). Realimentação Derivativa. Custo Garantido \mathcal{H}_∞ . Custo Garantido \mathcal{H}_2 . Custo Garantido Misto $\mathcal{H}_\infty/\mathcal{H}_2$. \mathcal{D} -estabilidade.

ABSTRACT

In this work, new conditions for the control of linear parameter-varying systems (LPV) are proposed, considering the state derivative feedback. At first, the \mathcal{H}_∞ problem will be addressed in order to derive conditions for the \mathcal{H}_∞ gain scheduling state derivative feedback controller. Then, conditions for the \mathcal{H}_2 gain scheduling state derivative feedback controller are obtained. The design of the controllers is based on linear matrix inequalities (LMIs). It is important to emphasise that \mathcal{D} -stability in the control project will also be considered, as a way to obtain good performance with a control signal that can be implemented in a real system. Here, the conditions for \mathcal{D} -stability will be treated in the sense of time-invariant systems, with "frozen" values of the parameter-varying in their range. In addition, the proposed conditions take into account a common quadratic Lyapunov function (CQLF) to then be compared with the proposed conditions considering a parameter-dependent Lyapunov function (PDLF). This work also offers necessary and sufficient conditions for the mixed $\mathcal{H}_\infty/\mathcal{H}_2$ control, i.e., it joins both \mathcal{H}_∞ problem and \mathcal{H}_2 problem. The proposed conditions are applied in several examples to show that using them it is possible to decrease the guaranteed cost \mathcal{H}_∞ and \mathcal{H}_2 , i.e, to minimise the effect of a possible disturbance in the system. In addition, through an unstable system, it is possible to stabilise the system and minimise the guaranteed cost with the proposed conditions.

Keywords: Linear Matrix Inequalities (LMIs). *Gain scheduling* (GS). State Derivative Feedback (SDF). \mathcal{H}_∞ Guaranteed Cost. \mathcal{H}_2 Guaranteed Cost. Mixed $\mathcal{H}_\infty/\mathcal{H}_2$ Guaranteed Cost. \mathcal{D} -stability.

LIST OF FIGURES

Figura 3.1	Model of an active suspension system.	38
Figura 3.2	Bode diagram for the system (3.29) in open-loop and in closed-loop. . .	41
Figura 3.3	Disturbance signal $w(t)$ as a sinusoidal scan (black solid line); transient response of the controlled output in open-loop (blue dotted line), and in closed-loop with the \mathcal{H}_∞ -GS-SDF controller (red solid line); and control signal for the \mathcal{H}_∞ -GS-SDF controller (green solid line).	42
Figura 3.4	Disturbance signal $w(t)$ as a square wave (black solid line); transient response of the controlled output in open-loop (blue dotted line), and in closed-loop with the \mathcal{H}_∞ -GS-SDF controller (red solid line); and control signal for the \mathcal{H}_∞ -GS-SDF controller (green solid line).	42
Figura 3.5	(a) Comparison between the \mathcal{H}_∞ guaranteed cost (dotted red line) and the \mathcal{H}_∞ real cost (solid black line) for the \mathcal{H}_∞ -GS-SDF controller, considering the sinusoidal scan; (b) A better view of the real cost; (c) Comparison between the open-loop real cost (dotted blue line) and the closed-loop real cost (solid black line).	43
Figura 3.6	(a) Comparison between the \mathcal{H}_∞ guaranteed cost (dotted red line) and the \mathcal{H}_∞ real cost (solid black line) for the \mathcal{H}_∞ -GS-SDF controller, considering the square wave; (b) A better view of the real cost; (c) Comparison between the open-loop real cost (dotted blue line) and the closed-loop real cost (solid black line).	44
Figura 3.7	Comparison between Theorems 3.1 (dotted red line) and 3.2 (solid black line).	45
Figura 3.8	Feasibility region obtained with Theorem 3.2.	46
Figura 3.9	Comparison between the guaranteed costs for Theorem 3.1 and Theorem 3.2.	47
Figura 4.1	Mass-spring-damper system.	59
Figura 4.2	Bode diagram for the system (4.47) in open-loop and in closed-loop. . .	61
Figura 4.3	Disturbance signal $w(t)$ as a sinusoidal scan (black solid line); transient response of the controlled output in open-loop (blue dotted line), and in closed-loop with the \mathcal{H}_2 -GS-SDF controller (red solid line); and control signal for \mathcal{H}_2 -GS-SDF controller (green solid line).	62

Figura 4.4	Disturbance signal $w(t)$ as a pulse (black solid line); transient response of the controlled output in open-loop (blue dotted line), and in closed-loop with the \mathcal{H}_2 -GS-SDF controller (red solid line); and control signal for \mathcal{H}_2 -GS-SDF controller (green solid line).	62
Figura 4.5	(a) Comparison between the \mathcal{H}_2 guaranteed cost (dotted red line and the \mathcal{H}_2 real cost (solid black line) for the \mathcal{H}_2 -GS-SDF controller, considering the sinusoidal scan; (b) A better view of the real cost; (c) Comparison between the open-loop real cost (dotted blue line) and the closed-loop real cost (solid black line).	63
Figura 4.6	(a) Comparison between the \mathcal{H}_2 guaranteed cost (dotted red line and the \mathcal{H}_2 real cost (solid black line) for the \mathcal{H}_2 -GS-SDF controller, considering the pulse; (b) A better view of the real cost; (c) Comparison between the open-loop real cost (dotted blue line) and the closed-loop real cost (solid black line).	63
Figura 4.7	(a) Comparison between Theorems 4.1 (dotted red line) and 4.2 (solid black line); (b) A better view of the \mathcal{H}_2 guaranteed cost for Theorem 4.2.	65
Figura 4.8	Feasibility region obtained with Theorem 4.2.	66
Figura 4.9	Comparison between the guaranteed costs for Theorem 4.1 and Theorem 4.2.	66
Figura 5.1	Region (q, \mathbb{R}) for pole placement.	69
Figura 5.2	Bode diagram for the system (3.29) in open-loop and in closed-loop.	74
Figura 5.3	Disturbance signal $w(t)$ as a sinusoidal scan (black solid line); transient response of the controlled output in closed-loop with the \mathcal{H}_∞ -GS-SDF controller (red dotted line), and in closed-loop with the \mathcal{D} - \mathcal{H}_∞ -GS-SDF controller (magenta solid line); and control signal for \mathcal{H}_∞ -GS-SDF controller (green dotted line) and control signal for \mathcal{D} - \mathcal{H}_∞ -GS-SDF controller (yellow solid line).	75
Figura 5.4	Disturbance signal $w(t)$ as a square wave (black solid line); transient response of the controlled output in closed-loop with the \mathcal{H}_∞ -GS-SDF controller (red dotted line), and in closed-loop with the \mathcal{D} - \mathcal{H}_∞ -GS-SDF controller (magenta solid line); and control signal for \mathcal{H}_∞ -GS-SDF controller (green dotted line) and control signal for \mathcal{D} - \mathcal{H}_∞ -GS-SDF controller (yellow solid line).	75

Figura 5.5	(a) Comparison between the \mathcal{H}_∞ guaranteed cost (dotted red line) and the \mathcal{H}_∞ real cost (solid black line) for the \mathcal{D} - \mathcal{H}_∞ -GS-SDF controller, considering the sinusoidal scan; (b) A better view of the real cost; (c) Comparison between the open-loop real cost (dotted blue line) and the closed-loop real cost (solid black line).	76
Figura 5.6	(a) Comparison between the \mathcal{H}_∞ guaranteed cost (dotted red line) and the \mathcal{H}_∞ real cost (solid black line) for the \mathcal{D} - \mathcal{H}_∞ -GS-SDF controller, considering the square wave; (b) A better view of the real cost; (c) Comparison between the open-loop real cost (dotted blue line) and the closed-loop real cost (solid black line).	76
Figura 5.7	Bode diagram for the system (4.47) in open-loop and in closed-loop. . .	78
Figura 5.8	Disturbance signal $w(t)$ as a sinusoidal scan (black solid line); transient response of the controlled output in closed-loop with the \mathcal{H}_2 -GS-SDF controller (red dotted line), and in closed-loop with the \mathcal{D} - \mathcal{H}_2 -GS-SDF controller (magenta solid line); and control signal for \mathcal{H}_2 -GS-SDF controller (green dotted line) and control signal for \mathcal{D} - \mathcal{H}_2 -GS-SDF controller (yellow solid line).	79
Figura 5.9	Disturbance signal $w(t)$ as a pulse (black solid line); transient response of the controlled output in closed-loop with the \mathcal{H}_2 -GS-SDF controller (red dotted line), and in closed-loop with the \mathcal{D} - \mathcal{H}_2 -GS-SDF controller (magenta solid line); and control signal for \mathcal{H}_2 -GS-SDF controller (green dotted line) and control signal for \mathcal{D} - \mathcal{H}_2 -GS-SDF controller (yellow solid line).	79
Figura 5.10	Comparison between the \mathcal{H}_2 guaranteed cost (dotted red line) and the \mathcal{H}_2 real cost (solid magenta line) for the \mathcal{D} - \mathcal{H}_2 -GS-SDF controller, considering the sinusoidal scan; A better view of the closed-loop real cost; Comparison between the closed-loop real cost with the \mathcal{H}_2 -GS-SDF controller (black dotted line) and the closed-loop real cost with the \mathcal{D} - \mathcal{H}_2 -GS-SDF controller (solid magenta line).	80
Figura 5.11	Comparison between the \mathcal{H}_2 guaranteed cost (dotted red line) and the \mathcal{H}_2 real cost (solid magenta line) for the \mathcal{D} - \mathcal{H}_2 -GS-SDF controller, considering the pulse; A better view of the closed-loop real cost; Comparison between the closed-loop real cost with the \mathcal{H}_2 -GS-SDF controller (black dotted line) and the closed-loop real cost with the \mathcal{D} - \mathcal{H}_2 -GS-SDF controller (solid magenta line).	80

Figura 6.1	Mass-spring-damper system.	86
Figura 6.2	Bode diagram for the system (6.1) in open-loop and in closed-loop. . .	87
Figura 6.3	Cloud of eigenvalues of the system (6.1) with controller (6.10).	88
Figura 6.4	Bode diagram for the system (6.1) in open-loop and in closed-loop. . .	89
Figura 6.5	Cloud of eigenvalues of the system (6.1) with controller (6.10).	89
Figura 6.6	Disturbance signal $w(t)$ as a sinusoidal scan (black solid line); transient response of the controlled output in open-loop (blue dotted line), and in closed-loop with the $\mathcal{D}\text{-}\mathcal{H}_2/\mathcal{H}_\infty$ -GS-SDF controller (red solid line); and control signal for the $\mathcal{D}\text{-}\mathcal{H}_2/\mathcal{H}_\infty$ -GS-SDF controller (green solid line).	90
Figura 6.7	Disturbance signal $w(t)$ as a square wave (black solid line); transient response of the controlled output in open-loop (blue dotted line), and in closed-loop with the $\mathcal{D}\text{-}\mathcal{H}_2/\mathcal{H}_\infty$ -GS-SDF controller (red solid line); and control signal for the $\mathcal{D}\text{-}\mathcal{H}_2/\mathcal{H}_\infty$ -GS-SDF controller (green solid line).	90
Figura 6.8	Disturbance signal $w(t)$ as a pulse (black solid line); transient response of the controlled output in open-loop (blue dotted line), and in closed-loop with the $\mathcal{D}\text{-}\mathcal{H}_2/\mathcal{H}_\infty$ -GS-SDF controller (red solid line); and control signal for the $\mathcal{D}\text{-}\mathcal{H}_2/\mathcal{H}_\infty$ -GS-SDF controller (green solid line). . .	91
Figura 6.9	(a) Comparison between the mixed $\mathcal{H}_2/\mathcal{H}_\infty$ guaranteed cost (dotted red line) and the mixed $\mathcal{H}_2/\mathcal{H}_\infty$ real cost (solid black line) for the $\mathcal{D}\text{-}\mathcal{H}_2/\mathcal{H}_\infty$ -GS-SDF controller, considering the sinusoidal scan; (b) A better view of the real cost; (c) Comparison between the open-loop real cost (dotted blue line) and the closed-loop real cost (solid black line). . .	91
Figura 6.10	(a) Comparison between the mixed $\mathcal{H}_2/\mathcal{H}_\infty$ guaranteed cost (dotted red line) and the mixed $\mathcal{H}_2/\mathcal{H}_\infty$ real cost (solid black line) for the $\mathcal{D}\text{-}\mathcal{H}_2/\mathcal{H}_\infty$ -GS-SDF controller, considering the square wave; (b) A better view of the real cost; (c) Comparison between the open-loop real cost (dotted blue line) and the closed-loop real cost (solid black line).	92
Figura 6.11	(a) Comparison between the mixed $\mathcal{H}_2/\mathcal{H}_\infty$ guaranteed cost (dotted red line) and the mixed $\mathcal{H}_2/\mathcal{H}_\infty$ real cost (solid black line) for the $\mathcal{D}\text{-}\mathcal{H}_2/\mathcal{H}_\infty$ -GS-SDF controller, considering the pulse; (c) Comparison between the open-loop real cost (dotted blue line) and the closed-loop real cost (solid black line).	92

Figura 6.12	Mixed $\mathcal{H}_2/\mathcal{H}_\infty$ guaranteed cost for Theorem 6.1 (dotted blue line) and for Theorem 6.2 (solid black line).	94
Figura 6.13	Feasibility region for Theorem 6.2.	95
Figura 7.1	(a) The simulation with 0.2 Hz of frequency; (b) The simulation with 2 Hz of frequency.	96
Figura 7.2	The $\alpha_1(t)$ and $\alpha_2(t)$ parameters for (a) 0.2 Hz, and (b) 2 Hz.	97
Figura 7.3	(a) The simulation with 0.1 Hz of frequency; (b) The simulation with 2 Hz of frequency.	102
Figura 7.4	The $\alpha_1(t)$ and $\alpha_2(t)$ parameters for (a) 0.1 Hz, and (b) 2 Hz.	103

LIST OF TABLES

Table 3.1	Quarter vehicle suspension system parameters.	39
Table 3.2	Eigenvalues of system (3.41) for controller (3.42).	45
Table 4.1	Mass-spring-damper parameters (CABELLO, 2009).	59
Table 4.2	Eigenvalues of system (4.54) for controller (4.55).	64
Table 5.1	Eigenvalues of system (3.41) for controller (5.22).	77
Table 5.2	Eigenvalues of system (4.54) for controller (5.24).	81
Table 6.1	Parameters of the mass-spring-damper system with one mass.	85
Table 6.2	Eigenvalues of system (4.54) for controllers (6.12) and (6.13).	93

LIST OF ABBREVIATIONS AND ACRONYMS

ARE	Algebraic Ricatti Equation
CQLFs	Common Quadratic Lyapunov Functions
DOF	Dynamical Output Feedback
GS	Gain Scheduling
LMIs	Linear Matrix Inequalities
LPV	Linear Parameter-Varying
LQR	Linear Quadratic
LTI	Linear Time-Invariant
MatLab [®]	MATrix LABoratory
PDLFs	Parameter-Dependent Lyapunov Functions
PID	Proportional-Integral-Derivative
SDF	State Derivative Feedback
SDOH	Sub-Domain Optimisation Heuristic
SF	State Feedback
T-S	Takagi-Sugeno

LIST OF SYMBOLS

©	Copyright
$diag(.,.,.,.,.)$	Diagonal matrix with properly dimensions
T	Transpose of a vector or matrix
$-T$	Inverse of a transpose matrix
*	Transpose block of a symmetric matrix
0	Null matrix with properly dimensions
I	Identity matrix with properly dimensions
\wedge_r	Unitary simplex for $\alpha(t)$
\wedge_r^d	Unitary simplex for $\dot{\alpha}(t)$
ρ_l	Upper bound for the derivative of $\alpha(t)$
$M < 0$ ($M \leq 0$)	Negative definite matrices (semi-definite)
$M > 0$ ($M \geq 0$)	Positive definite matrices (semi-definite)
$det(M)$	Determinant of M
$M(\alpha(t))$	Time-varying matrix
$\ \cdot \ $	Euclidean vector norm
r	Number of polytope vertices
\mathbb{R}	Set of real numbers
$\mathbb{R}^{n \times m}$	Set of the real matrices with dimension $n \times m$
γ	\mathcal{H}_∞ guaranteed cost
κ	\mathcal{H}_2 guaranteed cost
$\sum_{i=1}^j (\cdot)$	A sum from $i = 1$ to j
®	Trademark
∈	Belongs to
∀	For all
$\ x(t)\ _2$	Norm 2 of $x(t) \in \mathbb{R}^n$, given by $\ x(t)\ _2 = \sqrt{\int_0^\infty x(t)^T x(t) dt}$
\mathcal{L}_2	Space of measurable $x(t)$ Lebesgue signals satisfying $\ x(t)\ _\infty$

SUMMARY

1	INTRODUCTION	13
1.1	CONTRIBUTIONS	16
1.2	STRUCTURE OF THE TEXT	17
2	FUNDAMENTAL CONCEPTS AND PROPERTIES	19
3	\mathcal{H}_∞ GUARANTEED COST GAIN SCHEDULING STATE DERIVATIVE FEEDBACK	28
3.1	\mathcal{H}_∞ GAIN SCHEDULING STATE DERIVATIVE FEEDBACK WITH $P(\alpha(t))$	30
3.2	EXAMPLES	37
3.2.1	Example 3.1 - Active Suspension System	37
3.2.2	Example 3.2 - Unstable System	43
3.2.3	Example 3.3 - Analysis of the parameter ρ_l	45
3.2.4	Example 3.4 - Feasibility Analysis	46
4	\mathcal{H}_2 GUARANTEED COST GAIN SCHEDULING STATE DERIVATIVE FEEDBACK	48
4.1	\mathcal{H}_2 GAIN SCHEDULING STATE DERIVATIVE FEEDBACK WITH $P(\alpha(t))$	51
4.2	EXAMPLES	58
4.2.1	Example 4.1 - Mass-Spring-Damper System	58
4.2.2	Example 4.2 - Unstable System	63
4.2.3	Example 4.3 - Analysis of the parameter ρ_l	64
4.2.4	Example 4.4 - Feasibility Analysis	65
5	\mathcal{D}-STABILITY FOR LPV SYSTEMS	68
5.1	\mathcal{D} - \mathcal{H}_∞ GAIN SCHEDULING STATE DERIVATIVE FEEDBACK	68
5.2	\mathcal{D} - \mathcal{H}_2 GAIN SCHEDULING STATE DERIVATIVE FEEDBACK	72
5.3	EXAMPLES	73
5.3.1	Example 5.1 - Active Suspension System	73
5.3.2	Example 5.2 - Unstable System	77
5.3.3	Example 5.3 - Mass-Spring-Damper System	77
5.3.4	Example 5.4 - Unstable System	78
5.4	CONCLUSIONS ON THE \mathcal{D} -STABILITY FOR LPV SYSTEMS	81

6	$\mathcal{H}_2/\mathcal{H}_\infty$ GUARANTEED COST GAIN SCHEDULING STATE DERIVATIVE FEEDBACK	82
6.1	\mathcal{D} - $\mathcal{H}_2/\mathcal{H}_\infty$ GAIN SCHEDULING STATE DERIVATIVE FEEDBACK	84
6.2	EXAMPLES	84
6.2.1	Example 6.1 - Mass-Spring-Damper System	85
6.2.2	Example 6.2 - Unstable System	93
6.2.3	Example 6.3 - Feasibility Analysis	94
7	COMMENTS ON THE PROPOSED RESULTS	96
7.1	COMMENTS ON THE \mathcal{H}_∞ -GS-SDF	96
7.2	COMMENTS ON THE \mathcal{H}_2 -GS-SDF	102
7.3	COMMENTS ON THE $\mathcal{H}_2/\mathcal{H}_\infty$ -GS-SDF	107
7.4	COMMENTS ON THE \mathcal{D} -STABILITY	108
8	CONCLUSIONS	110
8.1	FUTURE RESEARCH SUGGESTIONS	111
8.2	PUBLICATIONS	112
	REFERENCES	113

1 INTRODUCTION

In the past few years, the State Derivative Feedback (SDF) has gained close attention in the control literature as we can see in the several papers dealing with it. For instance, in the following problems: vibration control of landing gear components (KWAK; WASHINGTON; YEDAVALLI, 2002), bridge cables (DUAN; NI; KO, 2005), pole placement for linear systems (ABDELAZIZ; VALÁŠEK, 2004), uncertain linear systems (ASSUNÇÃO et al., 2007; ABDELAZIZ, 2009; FARIA et al., 2009), active suspension systems (REITHMEIER; LEITMANN, 2003; SILVA et al., 2013; SEVER et al., 2017; YAZICI; SEVER, 2017), linear quadratic regulator (BETETO et al., 2018; SEVER; YAZICI, 2019), design of SDF control laws in discrete time (ROSSI et al., 2018), adjustment of vehicle's attitude and motion (FALLAH et al., 2012), pitch motion control for a marine vehicle (BASTURK; ROSENTHAL; KRSTIC, 2014), control of discretised systems (LEANDRO; PEREIRA; KIENITZ, 2020), control of boost converters (FAISAL; LATHER, 2020), descriptor systems (DUAN; ZHANG, 2002; CARDIM et al., 2008), singular systems (ZAGHDOUD; SALHI; KSOURI, 2018), Takagi-Sugeno (T-S) *fuzzy* descriptor systems (BARBOSA; SOUZA; PALHARES, 2019; HE et al., 2020), robust PID controllers (VESELÏ; KÖRÖSI, 2019), \mathcal{H}_∞ for linear systems (SEVER; YAZICI, 2017), \mathcal{H}_∞ for uncertain linear systems (YAZICI; SEVER, 2018), \mathcal{H}_∞ T-S *fuzzy* systems (KAEWPRAEK; ASSAWINCHAICHOTE, 2016; HE et al., 2020; RUANGSANG; ASSAWINCHAICHOT, 2019), delayed hybrid descriptor systems (GUANGMING et al., 2019), gain scheduling (LLINS et al., 2017), delayed fractional-order multiagent systems (LIU et al., 2018), partial eigenvalue assignment for linear systems (ARAÚJO, 2019), among others.

The main characteristic of SDF is that the signals of second-derivative are available to feedback owing to the presence of accelerometers as sensors. With this type of sensors, the second-derivative signals represent the acceleration signals. According to Abdelaziz and Valášek (2004), it is possible to obtain the velocity signals by integrating the acceleration signals with good accuracy, but the same does not occurs with the displacement signals. In this way, the SDF is widely applied on vibration suppression control in mechanical systems, hence the fact that the second-derivative signals are acceleration and velocity. It is worth mentioning that when sensors directly measure state-derivatives the State Feedback (SF) does not always solve the problem (SUEUR, 2016), owing to the signal noise when being integrated twice. Therefore, the SDF has the advantage of solving the problem with simplicity, using the signal available for feedback and with lower gains (SUEUR, 2016; TSENG, 2009).

Additionally, owing to their simple structure and low cost, accelerometers have been applied to a large number of engineering problems (SABATO et al., 2016; KASPRZYK et al., 2017; ZHU et al., 2018).

As we can note, the SDF is used to solve a variety of engineering problems. Newly, Yazici and Sever (2018) proposed a robust \mathcal{H}_∞ SDF controller for an active suspension system. In system theory, \mathcal{H}_∞ norm is a very important performance index, which measures the system capacity to reject energy bounded disturbances (MONTAGNER et al., 2005). Additionally, the \mathcal{H}_∞ problem has been addressed by several papers, for instance, Carniato et al. (2018) developed a robust \mathcal{H}_∞ switched static output feedback controller for continuous-time switched linear systems with polytopic uncertainties; Oliveira et al. (2018) introduced a local \mathcal{H}_∞ switched controller design for a class of uncertain nonlinear plants described by T-S *fuzzy* models with unknown membership functions; Rosa, Morais and Oliveira (2018) investigated the problems of stabilisation and mixed $\mathcal{H}_2/\mathcal{H}_\infty$ reduced-order dynamic output-feedback control of discrete-time linear systems. Following the path of SDF and \mathcal{H}_∞ problem, Ren and Zhang (2010) developed a robust \mathcal{H}_∞ control for descriptor systems using a proportional plus derivative state feedback; Kaewpraek and Assawinchaichote (2016) introduced an \mathcal{H}_∞ *fuzzy* SF plus SDF control for photovoltaic systems based on Linear Matrix Inequalities (LMIs); Ruangsang and Assawinchaichot (2019) investigated the problem of a robust \mathcal{H}_∞ SF plus SDF control for a class of uncertain non-linear systems described by a T-S *fuzzy* model.

Highlighting the papers that deal with the the \mathcal{H}_∞ -SDF problem, note that they explore only Linear Time-Invariant (LTI) or *fuzzy* systems. Differently from what is presented in (REN; ZHANG, 2010; KAEWPRAEK; ASSAWINCHAICHOTE, 2016; YAZICI; SEVER, 2018; RUANGSANG; ASSAWINCHAICHOT, 2019), this work addresses the \mathcal{H}_∞ -SDF problem, but for Linear Parameter-Varying (LPV) systems, using the Gain Scheduling (GS) strategy with LMIs to solve the problem. In control literature, Llins et al. (2017) introduced the GS strategy for LPV systems considering the SDF. Earlier, Apkarian and Gahinet (1995), Montagner et al. (2005) started the study of the \mathcal{H}_∞ problem for LPV systems considering the GS strategy. Now, we intend to derive LMI conditions for \mathcal{H}_∞ -GS-SDF controllers. The main choice of the GS strategy relies on the great interest of the control research community on it. According to Rugh and Shamma (2000), Al-Jiboory and Zhu (2018) it is achievable improve the system performance by means of the GS strategy, accessing the scheduling parameters (in real-time) through measurements or estimations. The surveys Rugh and Shamma (2000), Wei et al. (2014) and the references therein contain a great background on GS strategy.

Regarding the GS strategy to solve the problem of the \mathcal{H}_∞ guaranteed cost for LPV systems, several papers addressed it in specialised literature. For instance, Montagner et al. (2005), Montagner and Peres (2006) developed LMI conditions for the design of \mathcal{H}_∞ -GS controllers

for LPV systems; Zhou, Zhang and Zheng (2009) addressed the problem of \mathcal{H}_∞ -GS filter design for a class of parameter-varying discrete-time systems using LMIs; Caigny et al. (2012) proposed LMIs conditions for GS dynamical output feedback (DOF) controllers and GS-DOF mixed $\mathcal{H}_\infty/\mathcal{H}_2$ controllers for discrete-time LPV systems; Rosa, Morais and Oliveira (2018) investigated the problems of stabilisation and mixed $\mathcal{H}_2/\mathcal{H}_\infty$ reduced-order dynamic output-feedback control of discrete-time linear systems using parameter-dependent LMIs. As we can note, the \mathcal{H}_∞ problem is successfully solved by the GS strategy, hence our motivation to develop the \mathcal{H}_∞ -GS-SDF controller.

In addition to the \mathcal{H}_∞ , the \mathcal{H}_2 control is quite considered in the control literature. For instance, in the following problems: parametric eigenstructure assignment for linear systems (WANG; LIANG; DUAN, 2006), SDF control of overhead crane systems (ALI, 2017), microsatellite attitude control (YANG; SUN, 2002), robust \mathcal{H}_2 and \mathcal{H}_∞ filters for uncertain linear systems (LACERDA; OLIVEIRA; PERES, 2011), discrete-time periodic systems (FARGES et al., 2007; PEAUCELLE; EBIHARA; ARZELIER, 2008), active suspension control (AGHAIE; AMIRIFAR, 2007), two-floors building model vibration control (SANTOS et al., 2007), control of parameter dependent systems (OLIVEIRA; SOUZA; TROFINO, 2000). With the \mathcal{H}_2 norm it is measured the Root-Mean-Square (RMS), in time domain, value of an impulse response or stationary white noise response (YANG; SUN, 2002). It is worth to mention that we are using LPV systems, which means that the \mathcal{H}_2 problem is considered in the parameter-dependent sense as \mathcal{H}_2 guaranteed cost. In this work, the definition to this problem is based on the results of (PAGANINI; FERON, 2000; SOUZA; TROFINO; OLIVEIRA, 2003; XIE, 2005), and will be better explored later in the text. Considering the \mathcal{H}_2 guaranteed cost for LPV systems, a great number of papers deal with: Xie (2005), Xie (2012) designed new LMIs formulations for the GS control of LPV systems in which the Lyapunov matrix is decoupled from the system matrices; Aouani et al. (2012) developed conditions based on LMIs for the robust stability and the \mathcal{H}_2 performance analysis of LPV systems subject to uncertainties and under polytopic structure; Cai et al. (2014) designed sufficient conditions for the \mathcal{H}_2 -GS-SF and \mathcal{H}_2 -GS dynamic output feedback controllers for LPV systems; Kang, Lee and Chung (2017) introduced an observer gain scheduling based on \mathcal{H}_2 filter for discrete-time LPV systems; Al-Jiboory and Zhu (2018) developed the static output-feedback GS control for LPV systems with scheduling parameters measures affected by uncertainties or noises; Palma, Morais and Oliveira (2020) designed a technique named Sub-Domain Optimisation Heuristic (SDOH) in order to obtain \mathcal{H}_2 controllers or filters that treat robust stability independently of performance.

Note that the above papers of the \mathcal{H}_2 guaranteed cost for LPV systems do not use the SDF in the problem. In fact, a few papers consider the SDF on the resolution of the \mathcal{H}_2 problem. For instance, Zaghdoud, Salhi and Ksouri (2015) proposed a proportional plus derivative feedback controller for continuous and discrete descriptor systems; Zaghdoud, Salhi and Ksouri (2018)

developed SDF controllers for LTI descriptor systems considering the \mathcal{H}_2 in terms of the Linear Quadratic (LQ) criteria; Ali (2017) derived an \mathcal{H}_2 optimal control using the SDF (the \mathcal{H}_2 problem is also in terms of the LQ criteria). In this work, unlike what is done in the mentioned papers, we consider the \mathcal{H}_2 problem for LPV systems. Then, following this scenario on \mathcal{H}_∞ and \mathcal{H}_2 problems, this work has three main objectives, derive LMI conditions for the \mathcal{H}_∞ -GS control using SDF, the \mathcal{H}_∞ -GS-SDF control; derive LMI conditions for the \mathcal{H}_2 -GS control using SDF, the \mathcal{H}_2 -GS-SDF control; and derive LMI conditions for the $\mathcal{H}_2/\mathcal{H}_\infty$ -GS control using SDF, the $\mathcal{H}_2/\mathcal{H}_\infty$ -GS-SDF control. Note that the controllers are derived in order to reduce the \mathcal{H}_∞ and \mathcal{H}_2 guaranteed costs for LPV systems. To the best of the author's knowledge, the conditions for the controllers mentioned above have not been published yet.

Additionally, a region in the left-half plane for pole location is considered. This region may assist us to improve the system performance and/or to reduce the control signal. The chosen region is the \mathcal{D} region, presented in (CHILALI; GAHINET, 1996), where the \mathcal{H}_∞ problem is also considered. It is important to emphasise that the eigenvalue constraints must be understood in the time-invariant sense, i.e., for "frozen" values of the varying-parameter in its range (KAJIWARA; APKARIAN; GAHINET, 1999; PUIG; BOLEA; BLESÁ, 2012). Furthermore, to derive the LMI conditions a Common Quadratic Lyapunov Function (CQLF) and a Parameter-Dependent Lyapunov Function (PDLF) will be used and compared. The use of a PDLF in the approach of LPV systems seems to lead to less conservative results (WU et al., 1996; OLIVEIRA; GEROMEL, 2005; SATO; PEAUCELLE, 2013; AL-JIBOORY; ZHU, 2018), hence the main motivation to use it.

1.1 CONTRIBUTIONS

The main contributions of this work are:

- Design of an \mathcal{H}_∞ -GS-SDF controller for LPV systems;
- Design of an \mathcal{H}_∞ -GS-SDF controller for LPV systems considering a PDLF;
- Design of an \mathcal{H}_2 -GS-SDF controller for LPV systems;
- Design of an \mathcal{H}_2 -GS-SDF controller for LPV systems considering a PDLF;
- Design of a controller considering the SDF and the \mathcal{D} -stability for LPV systems;
- Design of a \mathcal{D} - \mathcal{H}_∞ -GS-SDF controller for LPV systems;
- Design of a \mathcal{D} - \mathcal{H}_2 -GS-SDF controller for LPV systems;
- Design of an $\mathcal{H}_\infty/\mathcal{H}_2$ -GS-SDF controller for LPV systems;

- Design of an \mathcal{D} - $\mathcal{H}_\infty/\mathcal{H}_2$ -GS-SDF controller for LPV systems;
- Inclusion of a parallel with the robust control.

1.2 STRUCTURE OF THE TEXT

The work is organised as follows:

- Chapter 2 presents some fundamentals concepts and properties that will be used over the text: the LPV system, the SDF for LPV systems, and a characterisation of the dependent parameter (and its derivative) were presented, followed by the introduction of the \mathcal{H}_∞ and \mathcal{H}_2 problems in terms of parameter-dependent systems. Also we presented a couple of useful lemmas.
- Chapter 3 presents the conditions for the \mathcal{H}_∞ -GS-SDF controllers in terms of LMIs. It is important to mention that the first conditions obtained used a CQLF and, in the subsequent conditions for the \mathcal{H}_∞ problem, a PDLF was used. For illustration, the proposed conditions were applied in four examples. The first example shows that the \mathcal{H}_∞ -GS-SDF controllers performed well when applied on an active suspension system. The second example was considered just to indicate that the proposed conditions are able to reduce the \mathcal{H}_∞ guaranteed cost and stabilise an uncertain system. The third example is an analysis of the ρ_l parameter when a PDLF ($P(\alpha(t))$) is considered. With suitable values, it is possible to obtain low \mathcal{H}_∞ guaranteed cost values. The fourth example is concerned with the comparison between the conditions with a CQLF and those with a PDLF, i.e., a feasibility analysis was performed.
- In Chapter 4 we derived GS-SDF controllers considering the \mathcal{H}_2 guaranteed cost. To obtain the controllers, the conditions were based on the results of (SOUZA; TROFINO, 2006), and the first conditions take into account a CQLF to later consider a PDLF. To analyse the performance of the proposed conditions, four examples were used. At first, we consider a mass-spring-damper system. Second, an unstable system is used to show that the proposed \mathcal{H}_2 -GS-SDF controller is capable of to reduce the \mathcal{H}_2 guaranteed cost and stabilise the system. An analysis of the ρ_l parameter is presented in the third example. Finally, a feasibility analysis is showed comparing the conditions with a CQLF with those with a PDLF.
- Chapter 5 presents the conditions for the \mathcal{D} - \mathcal{H}_∞ -GS-SDF and \mathcal{D} - \mathcal{H}_2 -GS-SDF controllers in terms of LMIs. The chosen \mathcal{D} -region was a circular disk in complex plane with center $(-1, 0)$, radius \mathbb{r} and decay rate δ , with $q = \delta + \mathbb{r}$. Furthermore, in this work, the eigenvalue constraints must be understood in the time-invariant sense, i.e., for "frozen"

values of the varying-parameter in its range (KAJIWARA; APKARIAN; GAHINET, 1999; PUIG; BOLEA; BLESA, 2012). The conditions derived were based on a CQLF. For illustration, the proposed conditions were applied in some examples, according to the examples presented in previous sections.

- In Chapter 6 we derived GS-SDF controllers considering the mixed $\mathcal{H}_\infty/\mathcal{H}_2$ problem. The conditions are based on a CQLF. Furthermore, the \mathcal{D} - $\mathcal{H}_\infty/\mathcal{H}_2$ controller is also presented. Following the previous chapters, some examples are considered to show that the new conditions performed well.
- Chapter 7 presents some comments about the new conditions proposed in this thesis. Also, it presents a parallel with the robust control, showing some new conditions considering the SDF, the \mathcal{H}_∞ problem, the \mathcal{H}_2 problem, the mixed $\mathcal{H}_\infty/\mathcal{H}_2$ problem, and the \mathcal{D} -stability.
- Chapter 8 states the conclusions, as well as the related publications and suggestions for future works.

8 CONCLUSIONS

This work proposed methods for the gain scheduling control of linear parameter-varying systems subjects to a disturbance signal. Through the project, the gain scheduling strategy is considered, which has been gaining attention in the control community and, having access to the scheduling parameter in real time, it is possible to improve the performance of the system. Furthermore, the state derivative is used owing to the easy measurement of the second-derivative signals, once that the system has accelerometers as main sensors. In addition, to deal with the disturbance signal, two approaches were considered, the \mathcal{H}_2 and the \mathcal{H}_∞ guaranteed costs. With the proposed method, it is achievable to reduce the effects of the disturbance signal in the performance of the systems, improving the system working. Another important fact is that to derive the LMI conditions, the Lemma 2.7 was used. With this lemma it is possible to deal with the cross product between three parameter-dependent variables.

For illustration, some examples have been presented to demonstrate the effectiveness of the proposed methods. Considering the \mathcal{H}_∞ guaranteed cost, the first example consisted of applying the \mathcal{H}_∞ -GS-SDF controller to an active suspension system. This system was subject to two disturbance signals, a sinusoidal scan and a square wave. In both cases, the designed controller was able of mitigate the effect of the disturbance signal, ensuring a satisfactory closed-loop performance, increasing the comfort to the driver and minimising the mechanical stress to the suspension system. The second example, an uncertain system was used to show that with the proposed methods it is possible to ensure a low \mathcal{H}_∞ guaranteed cost and stabilise the unstable system. The third and the fourth examples are complementary. They present an analysis of the ρ_l parameter and a feasibility analysis between Theorems 3.1 and 3.2. With these analysis it can be seen that the use of a PDLF is less conservative than the use of a CQLF.

Regarding the \mathcal{H}_2 -GS-SDF controllers, similar analysis to \mathcal{H}_∞ -GS-SDF controller were performed, also considering four examples. The first example considers a mass-spring-damper system subject to two disturbance signals, a sinusoidal scan and a pulse occurring periodically. In both cases the designed controller was able to minimise the effect of the disturbance signal, ensuring a satisfactory closed-loop performance. With the second example, it was shown that the \mathcal{H}_2 -GS-SDF is capable of to minimise and to stabilise the \mathcal{H}_2 guaranteed cost of an unstable system. The third and the fourth examples presented the analysis of the ρ_l parameter and a feasibility analysis for the \mathcal{H}_2 -GS-SDF.

It is important to highlight that, although the conditions for the \mathcal{H}_2 -GS-SDF and \mathcal{H}_∞ -GS-SDF were based on (YAZICI; SEVER, 2018) and (SOUZA; TROFINO; OLIVEIRA, 2003),

respectively, the conditions considering $P(\alpha(t))$ (and the characterisation of $\dot{\alpha}(t)$ was based on the results from (MONTAGNER; PERES, 2006). In this way, the considerations made in (MONTAGNER; PERES, 2006) for ρ_l is valid in this work. Thus, the conditions with $P(\alpha(t))$ (obtained with a PDLF and with a suitable choice of ρ_l) always ensure a lower cost, or at least equal, than the conditions obtained through a CQLF.

Furthermore, in this work was also presented a region in the left-half plane for pole location to improve the system performance and/or to reduce the control signal. The chosen region would be the \mathcal{D} region, presented in (CHILALI; GAHINET, 1996). It is important to emphasise that the eigenvalue constraints must be understood in the time-invariant sense, i.e., for "frozen" values of the parameter in its range (KAJIWARA; APKARIAN; GAHINET, 1999; PUIG; BOLEA; BLESA, 2012). With the \mathcal{D} - \mathcal{H}_2 -GS-SDF and \mathcal{D} - \mathcal{H}_∞ -GS-SDF controllers, and the properly choice of the parameters \mathfrak{r} and δ , it is possible to achieve better transients responses. However, a more detailed analysis of the inclusion of the \mathcal{D} -stability would be interesting for LPV systems.

Finally, two topics were still addressed in this thesis. The first deals with the mixed $\mathcal{H}_\infty/\mathcal{H}_2$ control considering SDF, LPV systems and the \mathcal{D} -stability. Through the examples we saw that, for this case, if \mathcal{D} -stability was not considered, it would not be possible to implement a mixed $\mathcal{H}_\infty/\mathcal{H}_2$ controller, since the controller norm was high. With this, it was also noticed that the sub-optimal guaranteed cost was the best choice, since it was possible to implement the controller.

The second topic deals with the robust control. As the conditions are similar, a parallel was made between the robust control and the GS control. However, this topic only intends to demonstrate that the conditions are similar and that it is possible to obtain conditions for robust control considering the SDF, the \mathcal{D} -stability, the \mathcal{H}_∞ problem, the \mathcal{H}_2 problem and the mixed $\mathcal{H}_\infty/\mathcal{H}_2$ problem. In addition, it remains as a suggestion for future works to analyse and implement the proposed conditions for the robust case.

8.1 FUTURE RESEARCH SUGGESTIONS

The following suggestions encompass ideas for future works:

- Lemma 2.7 considers the cross product between three variables, and its results can be conservative. In this way, for future works, we intend to study and analyse the triple sum to derive less conservative LMI conditions;
- It would be interesting to make a study of how the frequency interferes in the proposed conditions, since we are considering $P(\alpha(t))$ and the derivative of the parameter-varying appears;

- A more detailed analysis regarding the inclusion of the \mathcal{D} -region for LPV systems would be interesting for LPV systems. In addition to this analysis, it would be opportune to study the use of a PDLF to derive the LMI conditions for the \mathcal{D} -GS-SDF controllers;
- Derive the conditions for the the mixed $\mathcal{H}_\infty/\mathcal{H}_2$ control considering a PDFL ($P(\alpha(t))$);
- Analyse and compare the conditions for the robust case, considering the SDF, the \mathcal{D} -stability, the \mathcal{H}_∞ problem, the \mathcal{H}_2 problem and the mixed $\mathcal{H}_\infty/\mathcal{H}_2$ problem.

8.2 PUBLICATIONS

BETETO, M. A. L.; ASSUNÇÃO, E.; TEIXEIRA, M. C. M. Design of an \mathcal{H}_∞ gain scheduling state derivative controller for linear parameter-varying systems. *International Journal of Control*, Taylor & Francis, p. 1-17, 2021.

BETETO, M. A. L.; ASSUNÇÃO, E.; TEIXEIRA, M. C. M.; SILVA, E. R. P.; BUZACHERO, L. F. S.; CAUN R. P. Less conservative conditions for robust LQR-state-derivative controller design: an LMI approach. *International Journal of Systems Science*, Taylor & Francis, p. 2518-2537, 2021.

GALVÃO, R. K. H.; TEIXEIRA, M. C. M.; SZULC, T.; ASSUNÇÃO, E.; BETETO, M. A. L. Comments on 'Less conservative conditions for robust LQR-state-derivative controller design: an LMI approach' and new sufficient LMI conditions for invertibility of a convex combination of matrices. *International Journal of Systems Science*, Taylor & Francis, p. 1-9, 2022.

SERENI, B.; BETETO, M. A. L.; ASSUNÇÃO, E.; TEIXEIRA, M. C. M. Pole placement LMI constraints for stability and transient performance of LPV systems with incomplete state measurement. *Journal of the Franklin Institute*, Elsevier, p. 837-858, 2022.

REFERENCES

- ABDELAZIZ, T. H. S. Robust pole assignment for linear time-invariant systems using state-derivative feedback. *Proceedings of the Institution of Mechanical Engineers, Part I: Journal of Systems and Control Engineering*, London, v. 223, n. 2, p. 187–199, 2009.
- ABDELAZIZ, T. H. S.; VALÁŠEK, M. Pole-placement for SISO linear systems by state-derivative feedback. *IEE Proceedings-Control Theory and Applications*, Stevenage, v. 151, n. 4, p. 377–385, 2004.
- AGHAIE, Z.; AMIRIFAR, R. \mathcal{H}_2 and \mathcal{H}_∞ controllers design for an active suspension system via Riccati equations and LMIs. In: IEEE. *Second International Conference on Innovative Computing, Information and Control (ICICIC 2007)*. 2007. p. 341–341.
- AL-JIBOORY, A. K.; ZHU, G. Static output-feedback robust gain-scheduling control with guaranteed \mathcal{H}_2 performance. *Journal of the Franklin Institute*, London, v. 355, n. 5, p. 2221–2242, 2018.
- AL-JIBOORY, A. K.; ZHU, G. G. Improved synthesis conditions for mixed $\mathcal{H}_2/\mathcal{H}_\infty$ gain-scheduling control subject to uncertain scheduling parameters. *International Journal of Control*, Abingdon, v. 90, n. 3, p. 580–598, 2017.
- ALI, H. I. \mathcal{H}_2 -optimal control synthesis using state derivative feedback. *Baghdad, Al-Nahrain Journal for Engineering Sciences*, v. 20, n. 5, p. 1057–1063, 2017.
- AOUANI, N.; SALHI, S.; KSOURI, M.; GARCIA, G. \mathcal{H}_2 analysis for LPV systems by parameter-dependent Lyapunov functions. *IMA Journal of Mathematical Control and Information*, Oxford, v. 29, n. 1, p. 63–78, 2012.
- APKARIAN, P.; ADAMS, R. J. Advanced gain-scheduling techniques for uncertain systems. In: *Advances in linear matrix inequality methods in control*. : SIAM, 2000. p. 209–228.
- APKARIAN, P.; GAHINET, P. A convex characterization of gain-scheduled \mathcal{H}_∞ controllers. *IEEE Transactions on Automatic Control*, Piscataway, v. 40, n. 5, p. 853–864, 1995.
- ARAÚJO, J. M. Partial eigenvalue assignment in linear time-invariant systems using state-derivative feedback and a left eigenvectors parametrization. *Proceedings of the Institution of Mechanical Engineers, Part I: Journal of Systems and Control Engineering*, London, v. 233, n. 8, p. 1085–1089, 2019.
- ASSUNÇÃO, E.; TEIXEIRA, M. C. M.; FARIA, F. A.; SILVA, N. A. P. D.; CARDIM, R. Robust state-derivative feedback LMI-based designs for multivariable linear systems. *International Journal of Control*, Abingdon, v. 80, n. 8, p. 1260–1270, 2007.
- BARBOSA, E. M. C.; SOUZA, F. de O.; PALHARES, R. M. LMI-based design of

- state-derivative feedback control for Takagi-Sugeno fuzzy descriptor systems. *Ouro Preto, Anais do 14° Simpósio Brasileiro de Automação Inteligente*, v. 5, p. 2, 2019.
- BASTURK, H. I.; ROSENTHAL, B.; KRSTIC, M. Pitch control design for tandem lifting body catamaran by aft lifting body actuation. *IEEE Transactions on Control Systems Technology*, IEEE, v. 23, n. 2, p. 700–707, 2014.
- BETETO, M. A. L.; ASSUNÇÃO, E.; TEIXEIRA, M. C. M. Design of an \mathcal{H}_∞ gain scheduling state derivative feedback controller for linear parameter-varying systems. *International Journal of Control*, Abingdon, p. 1–17, 2021.
- BETETO, M. A. L.; ASSUNÇÃO, E.; TEIXEIRA, M. C. M.; SILVA, E. R. P.; BUZACHERO, L. F. S.; CAUN, R. P. New design of robust LQR-state derivative controllers via LMIs. *IFAC-PapersOnLine*, Florianópolis, v. 51, n. 25, p. 422–427, 2018.
- BOYD, S.; GHAOUI, L. E.; FERON, E.; BALAKRISHNAN, V. *Linear matrix inequalities in system and control theory*. : Siam, 1994.
- CABELLO, R. V. C. *Controle \mathcal{H}_∞ de vibrações com restrições no esforço de controle*. Tese (Doutorado) — Universidade Estadual de Campinas, Faculdade de Engenharia Mecânica, Curso de Pós-Graduação em Mecânica, Campinas, 2009.
- CAI, G.; HU, C.; YIN, B.; HE, H.; HAN, X. Gain-scheduled \mathcal{H}_2 controller synthesis for continuous-time polytopic LPV systems. *Mathematical Problems in Engineering*, Hindawi, v. 2014, 2014.
- CAIGNY, J. D.; CAMINO, J. F.; OLIVEIRA, R. C. L. F.; PERES, P. L. D.; SWEVER, J. Gain-scheduled dynamic output feedback control for discrete-time LPV systems. *International Journal of Robust and Nonlinear Control*, Hoboken, v. 22, n. 5, p. 535–558, 2012.
- CARDIM, R.; TEIXEIRA, M. C. M.; ASSUNÇÃO, E.; FARIA, F. A. Control designs for linear systems using state-derivative feedback. *Systems, Structure and Control*, London, p. 1–28, 2008.
- CARNIATO, L. A.; CARNIATO, A. A.; TEIXEIRA, M. C. M.; CARDIM, R.; JUNIOR, E. I. M.; ASSUNÇÃO, E. Output control of continuous-time uncertain switched linear systems via switched static output feedback. *International Journal of Control*, Abingdon, p. 1–20, 2018.
- CAUN, R. da P.; ASSUNÇÃO, E.; TEIXEIRA, M. C. M. $\mathcal{H}_2/\mathcal{H}_\infty$ formulation of LQR controls based on LMI for continuous-time uncertain systems. *International Journal of Systems Science*, Abingdon, v. 52, n. 3, p. 612–634, 2020.
- CHANG, X.-H.; HONG, L.; FENG, Y.-F. \mathcal{H}_∞ control for continuous-time TS fuzzy systems using fuzzy Lyapunov functions: A LMI approach. In: IEEE. *2010 Chinese Control and Decision Conference*. 2010. p. 2519–2524.
- CHEN, C.; ZHANG, R.; ZHANG, Q.; LIU, L. Mixed $\mathcal{H}_2/\mathcal{H}_\infty$ guaranteed cost control for high speed elevator active guide shoe with parametric uncertainties. *Mechanics & Industry*, EDP Sciences, v. 21, n. 5, p. 502, 2020.
- CHEN, F.; GUO, L.; GONG, S.; LUO, G. The study on \mathcal{D} -stability of dynamic interval

systems based on robust state observers. In: IOP PUBLISHING. *IOP Conference Series: Earth and Environmental Science*. 2019. v. 234, n. 1, p. 012033.

CHILALI, M.; GAHINET, P. \mathcal{H}_∞ design with pole placement constraints: an LMI approach. *IEEE Transactions on automatic control*, Piscataway, v. 41, n. 3, p. 358–367, 1996.

DAAFOUZ, J.; BERNUSSOU, J. Parameter dependent Lyapunov functions for discrete time systems with time varying parametric uncertainties. *Systems & control letters*, Amsterdam, v. 43, n. 5, p. 355–359, 2001.

DUAN, G.-R.; ZHANG, X. Dynamical order assignment in linear descriptor systems via state derivative feedback. In: IEEE. *Proceedings of the 41st IEEE Conference on Decision and Control, 2002*. 2002. v. 4, p. 4533–4538.

DUAN, Y.; NI, Y.; KO, J. State-derivative feedback control of cable vibration using semiactive magnetorheological dampers. *Computer-Aided Civil and Infrastructure Engineering*, Hoboken, v. 20, n. 6, p. 431–449, 2005.

EMAM, M.; FAKHARIAN, A. Attitude tracking of quadrotor UAV via mixed $\mathcal{H}_2/\mathcal{H}_\infty$ controller: An LMI based approach. In: IEEE. *2016 24th Mediterranean Conference on Control and Automation (MED)*. 2016. p. 390–395.

ESTRADA-MANZO, V.; LENDEK, Z.; GUERRA, T. M. Generalized LMI observer design for discrete-time nonlinear descriptor models. *Neurocomputing*, Amsterdam, v. 182, p. 210–220, 2016.

FAISAL, M.; LATHER, J. S. State derivative feedback control for boost converter via linear matrix inequalities. In: IEEE. *2020 First IEEE International Conference on Measurement, Instrumentation, Control and Automation (ICMICA)*. 2020. p. 1–4.

FALLAH, S.; KHAJEPOUR, A.; FIDAN, B.; CHEN, S.-K.; LITKOUHI, B. Vehicle optimal torque vectoring using state-derivative feedback and linear matrix inequality. *IEEE Transactions on Vehicular Technology*, Piscataway, v. 62, n. 4, p. 1540–1552, 2012.

FARGES, C.; PEAUCELLE, D.; ARZELIER, D.; DAAFOUZ, J. Robust \mathcal{H}_2 performance analysis and synthesis of linear polytopic discrete-time periodic systems via LMIs. *Systems & Control Letters*, Amsterdam, v. 56, n. 2, p. 159–166, 2007.

FARIA, F. A.; ASSUNÇÃO, E.; TEIXEIRA, M. C. M.; CARDIM, R.; SILVA, N. A. P. D. Robust state-derivative pole placement LMI-based designs for linear systems. *International Journal of Control*, Taylor & Francis, v. 82, n. 1, p. 1–12, 2009.

GREEN, M.; LIMEBEER, D. J. N. *Linear robust control*. : Prentice-Hall: Englenwood Cliffs, NJ., 1995.

GUANGMING, Z.; GUOWEI, Z.; KUN, M.; JIANWEI, X.; HUASHENG, Z.; JUNSHENG, Z. Derivative state feedback controller designing for delayed hybrid descriptor systems. In: IEEE. *2019 Chinese Control Conference (CCC)*. 2019. p. 1473–1476.

HADDAD, W. M.; BERNSTEIN, D. S. Controller design with regional pole constraints. IEEE, 1992.

- HE, J.; XU, F.; WANG, X.; LIANG, B. Admissibility analysis and robust \mathcal{H}_∞ control for T-S fuzzy descriptor systems with structured parametric uncertainties. *IEEE Transactions on Fuzzy Systems*, Piscataway, 2020.
- HE, Z.; XIE, W. Quadratic \mathcal{H}_2 gain performance analysis of LPV systems with realization of parametric transfer function. In: IEEE. *Proceedings of the 33rd Chinese Control Conference*. 2014. p. 1788–1792.
- KAEWPRAEK, N.; ASSAWINCHAICHOTE, W. \mathcal{H}_∞ fuzzy state-feedback control plus state-derivative-feedback control synthesis for photovoltaic systems. *Asian Journal of Control*, Hoboken, v. 18, n. 4, p. 1441–1452, 2016.
- KAJIWARA, H.; APKARIAN, P.; GAHINET, P. LPV techniques for control of an inverted pendulum. *IEEE Control Systems Magazine*, Piscataway, v. 19, n. 1, p. 44–54, 1999.
- KANG, C. M.; LEE, S.-H.; CHUNG, C. C. Discrete-time LPV \mathcal{H}_2 observer for vehicle model-based state observer. In: IEEE. *2017 11th Asian Control Conference (ASCC)*. 2017. p. 1182–1187.
- KASPRZYK, J.; KRAUZE, P.; BUDZAN, S.; RZEPECKI, J. Vibration control in semi-active suspension of the experimental off-road vehicle using information about suspension deflection. *Archives of Control Sciences*, Gliwice, v. 27, n. 2, p. 251–261, 2017.
- KHOSROWJERDI, M. J.; NIKOUKHAH, R.; SAFARI-SHAD, N. A mixed $\mathcal{H}_2/\mathcal{H}_\infty$ approach to simultaneous fault detection and control. *Automatica*, Elsevier, v. 40, n. 2, p. 261–267, 2004.
- KWAK, S.-K.; WASHINGTON, G.; YEDAVALLI, R. K. Acceleration feedback-based active and passive vibration control of landing gear components. *Journal of Aerospace Engineering*, Reston, v. 15, n. 1, p. 1–9, 2002.
- LACERDA, M. J.; OLIVEIRA, R. C.; PERES, P. L. Robust \mathcal{H}_2 and \mathcal{H}_∞ filter design for uncertain linear systems via LMIs and polynomial matrices. *Signal Processing*, Elsevier, v. 91, n. 5, p. 1115–1122, 2011.
- LEANDRO, M. A. C.; PEREIRA, R. L.; KIENITZ, K. H. Robust state derivative feedback LMI-based designs for discretized systems. *Anais da Sociedade Brasileira de Automática*, v. 2, n. 1, 2020.
- LEITE, V. J.; PERES, P. L. Pole location control design of an active suspension system with uncertain parameters. *Vehicle System Dynamics*, Abingdon, v. 43, n. 8, p. 561–579, 2005.
- LIU, C.; SUN, Z. W.; SHI, K. K.; WANG, F. Mixed $\mathcal{H}_2/\mathcal{H}_\infty$ control approach and its application in satellite attitude control system. In: TRANS TECH PUBL. *International Journal of Engineering Research in Africa*. 2016. v. 25, p. 89–97.
- LIU, J.; QIN, K.; CHEN, W.; LI, P. Consensus of delayed fractional-order multiagent systems based on state-derivative feedback. *Complexity*, Hindawi, v. 2018, 2018.
- LLINS, L. I. H.; ASSUNÇÃO, E.; TEIXEIRA, M. C. M.; CARDIM, R.; CADALSO, M. R. R.; OLIVEIRA, D. R. d.; SILVA, E. R. P. da. Design of gain scheduling control using state derivative feedback. *Mathematical Problems in Engineering*, Hindawi, v. 2017, 2017.

- LÖFBERG, J. YALMIP: A toolbox for modeling and optimization in MATLAB. In: TAIPEI, TAIWAN. *Proceedings of the CACSD Conference*. 2004. v. 3.
- MEISAMI-AZAD, M.; MOHAMMADPOUR, J.; GRIGORIADIS, K. M. Upper bound mixed \mathcal{H}_2 - \mathcal{H}_∞ control and integrated design for collocated structural systems. In: IEEE. *2009 American Control Conference*. 2009. p. 4563–4568.
- MOHSENIPOUR, R.; JEGARKANDI, M. F. Robust \mathcal{D} -stability testing function for LTI fractional order interval systems. In: IEEE. *2018 IEEE Conference on Control Technology and Applications (CCTA)*. 2018. p. 1277–1282.
- MONTAGNER, V. F.; OLIVEIRA, R. C. L. F.; LEITE, V. J. S.; PERES, P. L. D. LMI approach for \mathcal{H}_∞ linear parameter-varying state feedback control. *IEE Proceedings-Control Theory and Applications*, Stevenage, v. 152, n. 2, p. 195–201, 2005.
- MONTAGNER, V. F.; PERES, P. L. D. Robust stability and \mathcal{H}_∞ performance of linear time-varying systems in polytopic domains. *International Journal of Control*, Taylor & Francis, v. 77, n. 15, p. 1343–1352, 2004.
- MONTAGNER, V. F.; PERES, P. L. D. State Feedback Gain Scheduling for Linear Systems With Time-Varying Parameters. *New York, Journal of Dynamic Systems, Measurement, and Control*, v. 128, n. 2, p. 365–370, 2006.
- MOREIRA, M. R.; JÚNIOR, E. I. M.; ESTEVES, T. T.; TEIXEIRA, M.; CARDIM, R.; ASSUNÇÃO, E.; FARIA, F. A. Stabilizability and disturbance rejection with state-derivative feedback. *Mathematical Problems in Engineering*, Hindawi, v. 2010, 2010.
- OLIVEIRA, D. R. de; TEIXEIRA, M. C. M.; ALVES, U. N. L. T.; SOUZA, W. A. de; ASSUNÇÃO, E.; CARDIM, R. On local \mathcal{H}_∞ switched controller design for uncertain T-S fuzzy systems subject to actuator saturation with unknown membership functions. *Fuzzy Sets and Systems*, Amsterdam, v. 344, p. 1–26, 2018.
- OLIVEIRA, J. D.; SOUZA, C. E. D.; TROFINO, A. \mathcal{H}_2 analysis and control of parameter dependent systems via LMIs and parameter dependent Lyapunov functions. *IFAC Proceedings Volumes*, Amsterdam, v. 33, n. 14, p. 191–196, 2000.
- OLIVEIRA, M. C. de; GEROMEL, J. C. A class of robust stability conditions where linear parameter dependence of the lyapunov function is a necessary condition for arbitrary parameter dependence. *Systems & Control Letters*, Amsterdam, v. 54, n. 11, p. 1131–1134, 2005.
- OLIVEIRA, M. C. de; SKELTON, R. E. Stability tests for constrained linear systems. In: *Perspectives in robust control*. : London, Springer, 2001. p. 241–257.
- PAGANINI, F.; FERON, E. Linear matrix inequality methods for robust \mathcal{H}_2 analysis: A survey with comparisons. In: *Advances in linear matrix inequality methods in control*. : Philadelphia, SIAM, 2000. p. 129–151.
- PALMA, J. M.; MORAIS, C. F.; OLIVEIRA, R. C. L. F. \mathcal{H}_2 control and filtering of discrete-time LPV systems exploring statistical information of the time-varying parameters. *Journal of the Franklin Institute*, Amsterdam, v. 357, n. 6, p. 3835–3864, 2020.

- PARKS, T. Manual for model 210/210a rectilinear control systems. *Bell Canyon: Educational Control Products*, 1999.
- PEAUCELLE, D.; EBIHARA, Y.; ARZELIER, D. Robust \mathcal{H}_2 performance of discrete-time periodic systems: LMIs with reduced dimensions. *IFAC Proceedings Volumes*, Amsterdam, v. 41, n. 2, p. 1348–1353, 2008.
- PUIG, V.; BOLEA, Y.; BLESÁ, J. Robust gain-scheduled smith PID controllers for second order LPV systems with time varying delay. *IFAC Proceedings Volumes*, Amsterdam, v. 45, n. 3, p. 199–204, 2012.
- REITHMEIER, E.; LEITMANN, G. Robust vibration control of dynamical systems based on the derivative of the state. *Archive of Applied Mechanics*, London, v. 72, n. 11, p. 856–864, 2003.
- REN, J.; ZHANG, Q. Robust \mathcal{H}_∞ control for uncertain descriptor systems by proportional-derivative state feedback. *International Journal of Control*, Abingdon, v. 83, n. 1, p. 89–96, 2010.
- REZENDE, J. C.; CARVALHO, L.; NETO, J. R.; COSTA, M. V.; FORTES, E. V.; MACEDO, L. H. LQR design using LMIs and the robust \mathcal{D} -stability criterion for low-frequency oscillation damping in power systems. In: IEEE. *2021 14th IEEE International Conference on Industry Applications (INDUSCON)*. 2021. p. 188–195.
- ROSA, T. E.; MORAIS, C. F.; OLIVEIRA, R. C. L. F. New robust LMI synthesis conditions for mixed $\mathcal{H}_2/\mathcal{H}_\infty$ gain-scheduled reduced-order DOF control of discrete-time LPV systems. *International Journal of Robust and Nonlinear Control*, Hoboken, v. 28, n. 18, p. 6122–6145, 2018.
- ROSSI, F. Q.; GALVÃO, R. K. H.; TEIXEIRA, M. C. M.; ASSUNÇÃO, E. Direct discrete time design of robust state derivative feedback control laws. *International Journal of Control*, Abingdon, v. 91, n. 1, p. 70–84, 2018.
- RUANGSANG, S.; ASSAWINCHAICHOT, W. Control of nonlinear markovian jump system with time varying delay via robust \mathcal{H}_∞ fuzzy state feedback plus state-derivative feedback controller. *International Journal of Control, Automation and Systems*, London, v. 17, n. 9, p. 2414–2429, 2019.
- RUGH, W. J.; SHAMMA, J. S. Research on gain scheduling. *Automatica*, Amsterdam, v. 36, n. 10, p. 1401–1425, 2000.
- SABATO, A.; FENG, M. Q.; FUKUDA, Y.; CARNI, D. L.; FORTINO, G. A novel wireless accelerometer board for measuring low-frequency and low-amplitude structural vibration. *IEEE Sensors Journal*, Piscataway, v. 16, n. 9, p. 2942–2949, 2016.
- SANDE, T. P. J. Van der; GYSEN, B. L. J.; BESSELINK, I. J.; PAULIDES, J. J. H.; LOMONOVA, E. A.; NIJMEIJER, H. Robust control of an electromagnetic active suspension system: Simulations and measurements. *Mechatronics*, Amsterdam, v. 23, n. 2, p. 204–212, 2013.
- SANTOS, R. B.; BUENO, D. D.; MARQUI, C. R.; JR, V. L. Active vibration control of a

- two-floors building model based on \mathcal{H}_2 and \mathcal{H}_∞ methodologies using linear matrix inequalities (LMIs). In: *International Modal Analysis Conference—XXV IMAC, Orlando, EUA*. 2007.
- SATO, M.; PEAUCELLE, D. Gain-scheduled output-feedback controllers using inexact scheduling parameters for continuous-time LPV systems. *Automatica*, Amsterdam, v. 49, n. 4, p. 1019–1025, 2013.
- SCHERER, C. W. Mixed $\mathcal{H}_2/\mathcal{H}_\infty$ control for time-varying and linear parametrically-varying systems. *International Journal of Robust and Nonlinear Control*, Hoboken, v. 6, n. 9-10, p. 929–952, 1996.
- SCHMIED, R.; COLANERI, P. Mixed $\mathcal{H}_2\text{--}\mathcal{H}_\infty$ control for automated highway driving. *Mechatronics*, Amsterdam, v. 57, p. 63–72, 2019.
- SCHOMIG, E.; SZNAIER, M.; LY, U.-L. Mixed $\mathcal{H}_2\text{--}\mathcal{H}_\infty$ control of multimodel plants. *Journal of Guidance, Control, and Dynamics*, v. 18, n. 3, p. 525–531, 1995.
- SERENI, B.; BETETO, M.; ASSUNÇÃO, E.; TEIXEIRA, M. Pole placement LMI constraints for stability and transient performance of LPV systems with incomplete state measurement. *Journal of the Franklin Institute*, Amsterdam, p. 837–858, 2022.
- SEVER, M.; SENDUR, H. S.; YAZICI, H.; ARSLAN, M. S. Electro hydraulic suspension system design with optimal state derivative feedback controller. *Eskisehir, Anadolu University Journal of Science and Technology A-Applied Sciences and Engineering*, v. 18, n. 4, p. 777–787, 2017.
- SEVER, M.; YAZICI, H. Active control of vehicle suspension system having driver model via \mathcal{L}_2 gain state derivative feedback controller. In: *IEEE. 2017 4th international conference on electrical and electronic engineering (ICEEE)*. 2017. p. 215–222.
- SEVER, M.; YAZICI, H. LMI-based designs for robust state and output derivative feedback guaranteed cost controllers in reciprocal state space form. *International Journal of Control*, Abingdon, v. 94, n. 8, p. 2224–2237, 2019.
- SILVA, E. R. P. da; ASSUNÇÃO, E.; TEIXEIRA, M. C. M.; BUZACHERO, L. F. S. Condições robustas para a \mathcal{D} -estabilização de sistemas lineares politópicos usando a realimentação derivativa. In: *CBA: Congresso Brasileiro de Automática*. 2012.
- SILVA, E. R. P. da; ASSUNÇÃO, E.; TEIXEIRA, M. C. M.; CARDIM, R. Robust controller implementation via state-derivative feedback in an active suspension system subjected to fault. In: *IEEE. 2013 conference on control and fault-tolerant systems (SysTol)*. 2013. p. 752–757.
- SOUZA, C. E. D.; TROFINO, A.; OLIVEIRA, J. D. Parametric Lyapunov function approach to \mathcal{H}_2 analysis and control of linear parameter-dependent systems. *IEE Proceedings-Control Theory and Applications*, Stevenage, v. 150, n. 5, p. 501–508, 2003.
- SOUZA, C. E. de; TROFINO, A. Gain-scheduled \mathcal{H}_2 controller synthesis for linear parameter varying systems via parameter-dependent Lyapunov functions. *International Journal of Robust and Nonlinear Control: IFAC-Affiliated Journal*, Hoboken, v. 16, n. 5, p. 243–257, 2006.
- SUEUR, C. Disturbance rejection with derivative state feedback. In: *9th International*

Conference on Integrated Modeling and Analysis in Applied Control and Automation, IMAACA. 2016. v. 16, p. 26–28.

TANAKA, K.; IKEDA, T.; WANG, H. O. Fuzzy regulators and fuzzy observers: relaxed stability conditions and LMI-based designs. *IEEE Transactions on fuzzy systems*, Piscataway, v. 6, n. 2, p. 250–265, 1998.

TOH, K.-C.; TODD, M. J.; TUTUNCU, R. H. SDPT3 - a matlab software package for semidefinite programming, version 1.3. *Optimization methods and software*, Amsterdam, v. 11, n. 1-4, p. 545–581, 1999.

TSENG, Y.-W. Vibration control of piezoelectric smart plate using estimated state derivatives feedback in reciprocal state space framework. *Gurgaon, International Journal of Control Theory and Applications*, v. 2, n. 1, p. 61–71, 2009.

TUAN, H. D.; APKARIAN, P.; NARIKIYO, T.; YAMAMOTO, Y. Parameterized linear matrix inequality techniques in fuzzy control system design. *IEEE Transactions on fuzzy systems*, Piscataway, v. 9, n. 2, p. 324–332, 2001.

TUTUNCU, R. H.; TOH, K.-C.; TODD, M. J. Solving semidefinite-quadratic-linear programs using SDPT3. *Mathematical programming*, London, v. 95, n. 2, p. 189–217, 2003.

VESELÛ, V.; KÖRÖSI, L. Robust PI-D controller design for uncertain linear polytopic systems using LMI regions and \mathcal{H}_2 performance. *IEEE Transactions on Industry Applications*, Piscataway, v. 55, n. 5, p. 5353–5359, 2019.

WANG, G.-S.; LIANG, B.; DUAN, G.-R. \mathcal{H}_2 -optimal control with regional pole assignment via state feedback. *International Journal of Control, Automation, and Systems*, London, v. 4, n. 5, p. 653–659, 2006.

WEI, G.; WANG, Z.; LI, W.; MA, L. A survey on gain-scheduled control and filtering for parameter-varying systems. *Discrete Dynamics in Nature and Society*, Hindawi, v. 2014, 2014.

WU, F.; YANG, X. H.; PACKARD, A.; BECKER, G. Induced \mathcal{L}_2 -norm control for LPV systems with bounded parameter variation rates. *International Journal of Robust and Nonlinear Control*, Wiley Online Library, v. 6, n. 9-10, p. 983–998, 1996.

WU, H.-N.; FENG, S.; LIU, Z.-Y.; GUO, L. Disturbance observer based robust mixed $\mathcal{H}_2/\mathcal{H}_\infty$ fuzzy tracking control for hypersonic vehicles. *Fuzzy Sets and Systems*, Amsterdam, v. 306, p. 118–136, 2017.

XIE, W. \mathcal{H}_2 gain scheduled state feedback for LPV system with new LMI formulation. *IEE Proceedings-Control Theory and Applications*, Stevenage, v. 152, n. 6, p. 693–697, 2005.

XIE, W. Multi-objective $\mathcal{H}_2/\mathcal{L}_2$ performance controller synthesis for LPV systems. *Asian Journal of Control*, Wiley Online Library, v. 14, n. 5, p. 1273–1281, 2012.

YANG, C.-D.; SUN, Y.-P. Mixed $\mathcal{H}_2/\mathcal{H}_\infty$ cruise controller design for high speed train. *International Journal of control*, Abingdon, v. 74, n. 9, p. 905–920, 2001.

YANG, C.-D.; SUN, Y.-P. Mixed $\mathcal{H}_2/\mathcal{H}_\infty$ state-feedback design for microsatellite attitude

- control. *Control Engineering Practice*, Amsterdam, v. 10, n. 9, p. 951–970, 2002.
- YAZICI, H.; SEVER, M. Output derivative feedback vibration control of an integrated vehicle suspension system. *Proceedings of the institution of mechanical engineers, part I: Journal of systems and control engineering*, London, p. 409–419, 2017.
- YAZICI, H.; SEVER, M. \mathcal{L}_2 gain state derivative feedback control of uncertain vehicle suspension systems. *Journal of Vibration and Control*, London, v. 24, n. 16, p. 3779–3794, 2018.
- YU, J.-T. A new static output feedback approach to the suboptimal mixed $\mathcal{H}_2/\mathcal{H}_\infty$ problem. *International Journal of Robust and Nonlinear Control: IFAC-Affiliated Journal*, v. 14, n. 12, p. 1023–1034, 2004.
- ZAGHDOUD, R.; SALHI, S.; KSOURI, M. On proportional plus derivative state feedback \mathcal{H}_2 control for descriptor systems. In: *Handbook of Research on Advanced Intelligent Control Engineering and Automation*. : Hershey, IGI Global, 2015. p. 146–172.
- ZAGHDOUD, R.; SALHI, S.; KSOURI, M. State derivative feedback for singular systems. *IMA Journal of Mathematical Control and Information*, Oxford, v. 35, n. 2, p. 611–626, 2018.
- ZHOU, S.; ZHANG, B.; ZHENG, W. X. Gain-scheduled \mathcal{H}_∞ filtering of parameter-varying discrete-time systems via parameter-dependent lyapunov functions. *International Journal of Control, Automation and Systems*, London, v. 7, n. 3, p. 475–479, 2009.
- ZHU, Q.; LI, L.; CHEN, C.-J.; LIU, C.-Z.; HU, G.-D. A low-cost lateral active suspension system of the high-speed train for ride quality based on the resonant control method. *IEEE Transactions on Industrial Electronics*, Piscataway, v. 65, n. 5, p. 4187–4196, 2018.